# FLOOD INSURANCE STUDY FEDERAL EMERGENCY MANAGEMENT AGENCY

## VOLUME 1 OF 3



## SANTA CRUZ COUNTY, CALIFORNIA AND INCORPORATED AREAS

COMMUNITY NAME	COMMUNITY NUMBER
CAPITOLA, CITY OF	060354
SANTA CRUZ, CITY OF	060355
SANTA CRUZ COUNTY UNINCORPORATED AREAS	060353
SCOTTS VALLEY, CITY OF	060356
WATSONVILLE, CITY OF	060357



## REVISED: SEPTEMBER 29, 2017

FLOOD INSURANCE STUDY NUMBER 06087CV001C

Version Number 2.3.2.0

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Flood Profiles	Panel
Aptos Creek	01-03 P
Arana Gulch	04-06 P
Carbonera Creek	07-15 P
Corralitos Creek	16-19 P
Coward Creek	20-21 P
Harkins Slough	22-23 P
Moore Creek	24-26 P
Nobel Creek	27-28 P

#### Volume 3 – SEPTEMBER 29, 2017 Exhibits

Flood Profiles	Panel
Pajaro River	29-36 P
Pajaro River – without consideration of	37-44 P
Levee	
Rodeo Creek Gulch	45-46 P
Salsipuedes Creek	47-48 P
Salsipuedes Creek – without consideration	49-50 P
of Left Levee	- / -
Salsipuedes Creek – without consideration of Right Levee	51 P
San Lorenzo River	52-62 P
San Lorenzo River – without consideration	63-64 P
of Levee	
San Vicente Creek	65 P
Schwans Lagoon	66 P
Soquel Creek	67-70 P
Struve Slough	71-73 P
Thomasello Creek	74 P
Thompson Creek	75 P
Watsonville Slough	76-84 P
Zayante Creek	85-89 P

#### **Published Separately**

Flood Insurance Rate Map (FIRM)

#### FLOOD INSURANCE STUDY REPORT SANTA CRUZ COUNTY, CALIFORNIA

#### **SECTION 1.0 – INTRODUCTION**

#### 1.1 The National Flood Insurance Program

The National Flood Insurance Program (NFIP) is a voluntary Federal program that enables property owners in participating communities to purchase insurance protection against losses from flooding. This insurance is designed to provide an alternative to disaster assistance to meet the escalating costs of repairing damage to buildings and their contents caused by floods.

For decades, the national response to flood disasters was generally limited to constructing floodcontrol works such as dams, levees, sea-walls, and the like, and providing disaster relief to flood victims. This approach did not reduce losses nor did it discourage unwise development. In some instances, it may have actually encouraged additional development. To compound the problem, the public generally could not buy flood coverage from insurance companies, and building techniques to reduce flood damage were often overlooked.

In the face of mounting flood losses and escalating costs of disaster relief to the general taxpayers, the U.S. Congress created the NFIP. The intent was to reduce future flood damage through community floodplain management ordinances, and provide protection for property owners against potential losses through an insurance mechanism that requires a premium to be paid for the protection.

The U.S. Congress established the NFIP on August 1, 1968, with the passage of the National Flood Insurance Act of 1968. The NFIP was broadened and modified with the passage of the Flood Disaster Protection Act of 1973 and other legislative measures. It was further modified by the National Flood Insurance Reform Act of 1994 and the Flood Insurance Reform Act of 2004. The NFIP is administered by the Federal Emergency Management Agency (FEMA), which is a component of the Department of Homeland Security (DHS).

Participation in the NFIP is based on an agreement between local communities and the Federal Government. If a community adopts and enforces floodplain management regulations to reduce future flood risks to new construction and substantially improved structures in Special Flood Hazard Areas (SFHAs), the Federal Government will make flood insurance available within the community as a financial protection against flood losses. The community's floodplain management regulations must meet or exceed criteria established in accordance with Title 44 Code of Federal Regulations (CFR) Part 60.3, *Criteria for land Management and Use*.

SFHAs are delineated on the community's Flood Insurance Rate Maps (FIRMs). Under the NFIP, buildings that were built before the flood hazard was identified on the community's FIRMs are generally referred to as "Pre-FIRM" buildings. When the NFIP was created, the U.S. Congress recognized that insurance for Pre-FIRM buildings would be prohibitively expensive if the premiums were not subsidized by the Federal Government. Congress also recognized that most of these flood prone buildings were built by individuals who did not have sufficient knowledge of the flood hazard to make informed decisions. The NFIP requires that full actuarial rates reflecting the complete flood risk be charged on all buildings constructed or substantially improved on or after the effective date of the initial FIRM for the community or after December 31, 1974, whichever is later. These buildings are generally referred to as "Post-FIRM" buildings.

#### 1.2 Purpose of this Flood Insurance Study Report

This Flood Insurance Study (FIS) report revises and updates information on the existence and severity of flood hazards for the study area. The studies described in this report developed flood hazard data that will be used to establish actuarial flood insurance rates and to assist communities in efforts to implement sound floodplain management.

In some states or communities, floodplain management criteria or regulations may exist that are more restrictive than the minimum Federal requirements. Contact your State NFIP Coordinator to ensure that any higher State standards are included in the community's regulations.

#### 1.3 Jurisdictions Included in the Flood Insurance Study Project

This FIS Report covers the entire geographic area of Santa Cruz County, California.

The jurisdictions that are included in this project area, along with the Community Identification Number (CID) for each community and the 8-digit Hydrologic Unit Codes (HUC-8) sub-basins affecting each, are shown in Table 1. The Flood Insurance Rate Map (FIRM) panel numbers that affect each community are listed. If the flood hazard data for the community is not included in this FIS Report, the location of that data is identified.

Community	CID	HUC-8 Sub- Basin(s)	Located on FIRM Panel(s)	If Not Included, Location of Flood Hazard Data
Capitola, City Of	060354	18060015	06087C0351E 06087C0352F 06087C0353F 06087C0354F 06087C0356F	
Santa Cruz, City Of	060355	18050006, 18060015	06087C0219E 06087C0238E 06087C0327E <sup>1</sup> 06087C0329F 06087C0331E 06087C0332E 06087C0333F 06087C0334F 06087C0351E	
Santa Cruz County, Unincorporated Areas	060353	18050006, 18060002, 18060015	06087C0025E <sup>1</sup> 06087C0050E <sup>1</sup> 06087C0075E <sup>1</sup> 06087C0080E <sup>1</sup>	

Table 1: Listing of NFIP Jurisdictions

		HUC-8		If Not Included,
	015	Sub-	Located on FIRM	Location of Flood
Community	CID	Basin(s)		Hazard Data
			06087C0082E	
			06087C0083E	
			06087C0084E	
			06087C0090E	
			06087C0092E	
			06087C0094E	
			06087C0095E	
			06087C0105E	
			06087C0110E	
			06087C0113E	
			06087C0115E	
			06087C0120E	
			06087C0150E	
			06087C0156F	
			06087C0157F	
			06087C0159F	
			06087C0167F	
			06087C0180E	
			06087C0185E	
Santa Cruz Countv.	000050	18050006,	06087C0186F	
Unincorporated Areas	060353	18060002,	06087C0187F	
		10000013	06087C0188F	
			06087C0189F	
			06087C0193F	
			06087C0195F	
			06087C0201E	
			06087C0202E	
			06087C0203E	
			06087C0204E	
			06087C0214E	
			0608/C021/E	
			06087C0218E	
			06087C0219E	

		HUC-8		If Not Included,
	015	Sub-	Located on FIRM	Location of Flood
Community	CID	Basin(s)	Panel(s)	Hazard Data
			06087C0226E <sup>1</sup>	
			06087C0227E	
			06087C0228E	
			06087C0229E'	
			06087C0235E	
			06087C0236E	
			06087C0237E	
			06087C0238E	
			06087C0239E	
			06087C0245E	
			06087C0275E	
			06087C0300E <sup>1</sup>	
			06087C0306F	
			06087C0307F	
			06087C0309F	
			06087C0326F	
			06087C0327E <sup>1</sup>	
			06087C0328F	
			06087C0329F	
Santa Cruz County		18050006,	06087C0331E	
Unincorporated Areas,	060353	18060002,	06087C0332E	
continued		18060015	06087C0334F	
			06087C0351E	
			06087C0352F	
			06087C0353F	
			06087C0354F	
			06087C0356F	
			06087C0357F	
			06087C0358F	
			06087C0359F	
			06087C0378F	
			06087C0380F	
			06087C0381E	
			06087C0382E	
			06087C0383E	
			06087C0384E	
			06087C0386F	
			06087C0387F <sup>1</sup>	
			06087C0388F	
			06087C0389F	
			06087C0391E	

		HUC-8		If Not Included,
		Sub-	Located on FIRM	Location of Flood
Community	CID	Basin(s)		Hazard Data
			06087C0392E	
			06087C0393E	
			06087C0394E	
			06087C0403E	
		18050006	06087C0405E	
			06087C0410E	
			06087C0411E	
Santa Cruz County,	060353	18060002,	06087C0412E	
Unincorporated Areas		18060015	06087C0416E	
			06087C0417E	
			06087C0418E	
			06087C0419E	
			06087C0430E	
			06087C0440E	
			06087C0452F	
			06087C0456F	
			06087C0209E	
			06087C0216E	
			06087C0217E	
Scotts Valley, City Of	060356	18060015	06087C0218E	
			06087C0219E	
			06087C0228E	
			06087C0236E	
			06087C0275E	
			06087C0381E	
			06087C0383E	
			06087C0384E	
			06087C0387F <sup>1</sup>	
Watsonville, City Of	060357	18060002	06087C0391E	
			06087C0392E	
			06087C0393E	
			06087C0394E	
			06087C0411E	
			06087C0413E	

<sup>1</sup>Panel Not Printed

#### 1.4 Considerations for using this Flood Insurance Study Report

The NFIP encourages State and local governments to implement sound floodplain management programs. To assist in this endeavor, each FIS Report provides floodplain data, which may include a combination of the following: 10-, 4-, 2-, 1-, and 0.2-percent annual chance flood elevations (the 1% annual chance flood elevation is also referred to as the Base Flood Elevation

(BFE)); delineations of the 1% annual chance and 0.2% annual chance floodplains; and 1% annual chance floodway. This information is presented on the FIRM and/or in many components of the FIS Report, including Flood Profiles, Floodway Data tables, Summary of Non-Coastal Stillwater Elevations tables, and Coastal Transect Parameters tables (not all components may be provided for a specific FIS).

This section presents important considerations for using the information contained in this FIS Report and the FIRM, including changes in format and content. Figures 1, 2, and 3 present information that applies to using the FIRM with the FIS Report.

• Part or all of this FIS Report may be revised and republished at any time. In addition, part of this FIS Report may be revised by a Letter of Map Revision (LOMR), which does not involve republication or redistribution of the FIS Report. Refer to Section 6.5 of this FIS Report for information about the process to revise the FIS Report and/or FIRM.

It is, therefore, the responsibility of the user to consult with community officials by contacting the community repository to obtain the most current FIS Report components. Communities participating in the NFIP have established repositories of flood hazard data for floodplain management and flood insurance purposes. Community map repository addresses are provided in Table 31, "Map Repositories," within this FIS Report.

• New FIS Reports are frequently developed for multiple communities, such as entire counties. A countywide FIS Report incorporates previous FIS Reports for individual communities and the unincorporated area of the county (if not jurisdictional) into a single document and supersedes those documents for the purposes of the NFIP.

The initial Countywide FIS Report for Santa Cruz County became effective on March 2, 2006. Refer to Table 28 for information about subsequent revisions to the FIRMs.

• Previous FIS Reports and FIRMs may have included levees that were accredited as reducing the risk associated with the 1% annual chance flood based on the information available and the mapping standards of the NFIP at that time. For FEMA to continue to accredit the identified levees, the levees must meet the criteria of the Code of Federal Regulations, Title 44, Section 65.10 (44 CFR 65.10), titled "Mapping of Areas Protected by Levee Systems."

Since the status of levees is subject to change at any time, the user should contact the appropriate agency for the latest information regarding levees presented in Table 9 of this FIS Report. For levees owned or operated by the U.S. Army Corps of Engineers (USACE), information may be obtained from the USACE national levee database (nld.usace.army.mil). For all other levees, the user is encouraged to contact the appropriate local community.

• FEMA has developed a *Guide to Flood Maps* (FEMA 258) and online tutorials to assist users in accessing the information contained on the FIRM. These include how to read panels and step-by-step instructions to obtain specific information. To obtain this guide and other assistance in using the FIRM, visit the FEMA Web site at www.fema.gov/online-tutorials.

The FIRM Index in Figure 1 shows the overall FIRM panel layout within Santa Cruz County, and also displays the panel number and effective date for each FIRM panel in the county. Other information shown on the FIRM Index includes community boundaries, flooding sources, watershed boundaries, and United States Geological Survey (USGS) Hydrologic Unit Code-8 (HUC-8) codes.

				*002	?5E		S.	*008	50E Ra county	
						*0082E	*010	5E	*0110E	
*00	SAN MATEO COUNTY *0075E		UUSUE		*0083E	0084E 5/16/2012				
			*0090F		0095E	0092E 5/16/2012	0115E 5/16/2012		0120E 5/16/2012	
	S	HU( an Franc	C8 18050006 Isco Coastal Sout		5/16/2012 ]	0094E 5/16/2012	0113E 5/16/2012 HUC8 Mont		18060015 arey Bay	
***0155E	0156F 9/29/2017	0157F 9/29/2017	018	30E	*01955		0201E 5/16/2012	0202E 5/16/2012	0206E 5/16/2012	0207E 5/16/2012
	****0158F	0159F 9/29/2017	5/16/	2012 SANTA	CRUZ ( 060353	COUNT	0203E 5/16/2012 Y	0204E 5/16/2012	0208E 5/16/2012	0209E 5/16/2012
***01655		0167F 9/29/2017	0186F 9/29/2017	0187F 9/29/2017	*01	95F	*0211E	0212E 5/16/2012	0216E 5/16/2012	0217E 5/16/2012
	***0165E ***0170F		0188F 9/29/2017	0189F 9/29/2017	0193F 9/29/2017	₽-2	*0213E	*0214E	0218E 5/16/2012	0219E 5/16/2012
			***0	305F	0306F 9/29/2017	0307F 9/29/2017	0326F 9/29/2017 2-1	*0327E	0331E 5/16/2012 2	0332E 5/16/2012
					***0308F	0309F 9/29/2017	0328F 9/29/2017	0329F 9/29/2017	0333F 9/29/2017-	0334F 9/29/2017

best information available at the time of publication. As such, they may be more current than those shown on FIRM panels issued before September 29, 2017.

Key Number	Community	CID
1	City of Scotts Valley	060356
2	City of Santa Cruz	060355
·		1

***0315E	***0320E	***0340E	***0345E	



Map Projection: Universal Transverse Mercator Zone 10 North; North American Datum 1983

## THE INFORMATION DEPICTED ON THIS MAP AND SUPPORTING DOCUMENTATION ARE ALSO AVAILABLE IN DIGITAL FORMAT AT

#### HTTP://MSC.FEMA.GOV

SEE FLOOD INSURANCE STUDY FOR ADDITIONAL INFORMATION

\* PANEL NOT PRINTED - NO SPECIAL FLOOD HAZARD AREAS \*\* PANEL NOT PRINTED - AREA OUTSIDE COUNTY BOUNDARY \*\*\* PANEL NOT PRINTED - OPEN WATER AREA \*\*\*\* PANEL NOT PRINTED - AREA ALL WITHIN ZONE VE (EL 21)



#### NATIONAL FLOOD INSURANCE PROGRAM

FLOOD INSURANCE RATE MAP INDEX

## SANTA CRUZ COUNTY, CALIFORNIA and Incorporated Areas PANELS PRINTED:

 $\begin{array}{l} 0084, 0092, 0094, 0095, 0113, 0115, 0120, 0156, 0157, 0159, 0167, 0180, \\ 0186, 0187, 0188, 0189, 0193, 0201, 0202, 0203, 0204, 0206, 0207, 0208, \\ 0209, 0212, 0216, 0217, 0218, 0219, 0228, 0235, 0236, 0237, 0238, 0239, \\ 0245, 0275, 0306, 0307, 0309, 0326, 0328, 0329, 0331, 0332, 0333, 0334, \\ 0351, 0352, 0353, 0354, 0356, 0357, 0358, 0359, 0378, 0380, 0381, 0382, \\ 0383, 0384, 0386, 0388, 0389, 0391, 0392, 0393, 0394, 0403, 0405, 0411, \\ 0412, 0413, 0416, 0417, 0418, 0419, 0440, 0452, 0456 \end{array}$ 







**ATTENTION:** The corporate limits shown on this FIRM Index are based on the best information available at the time of publication. As such, they may be more current than those shown on FIRM panels issued before September 29, 2017.



Map Projection: Universal Transverse Mercator Zone 10 North; North American Datum 1983

## THE INFORMATION DEPICTED ON THIS MAP AND SUPPORTING DOCUMENTATION ARE ALSO AVAILABLE IN DIGITAL FORMAT AT

#### HTTP://MSC.FEMA.GOV

SEE FLOOD INSURANCE STUDY FOR ADDITIONAL INFORMATION

\* PANEL NOT PRINTED - NO SPECIAL FLOOD HAZARD AREAS \*\* PANEL NOT PRINTED - AREA OUTSIDE COUNTY BOUNDARY \*\*\* PANEL NOT PRINTED - OPEN WATER AREA



#### NATIONAL FLOOD INSURANCE PROGRAM

FLOOD INSURANCE RATE MAP INDEX

## SANTA CRUZ COUNTY, CALIFORNIA and Incorporated Areas PANELS PRINTED:

0084, 0092, 0094, 0095, 0113, 0115, 0120, 0156, 0157, 0159, 0167, 0180, 0186, 0187, 0188, 0189, 0193, 0201, 0202, 0203, 0204, 0206, 0207, 0208, 0209, 0212, 0216, 0217, 0218, 0219, 0228, 0235, 0236, 0237, 0238, 0239, 0245, 0275, 0306, 0307, 0309, 0326, 0328, 0329, 0331, 0332, 0333, 0334, 0351, 0352, 0353, 0354, 0356, 0357, 0358, 0359, 0378, 0380, 0381, 0382, 0383, 0384, 0386, 0388, 0389, 0391, 0392, 0393, 0394, 0403, 0405, 0411, 0412, 0413, 0416, 0417, 0418, 0419, 0440, 0452, 0456



Each FIRM panel may contain specific notes to the user that provide additional information regarding the flood hazard data shown on that map. However, the FIRM panel does not contain enough space to show all the notes that may be relevant in helping to better understand the information on the panel. Figure 2 contains the full list of these notes.

#### Figure 2: FIRM Notes to Users

## NOTES TO USERS

For information and questions about this map, available products associated with this FIRM including historic versions of this FIRM, how to order products, or the National Flood Insurance Program in general, please call the FEMA Flood Map Information eXchange at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA Map Service Center website at msc.fema.gov. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the website. Users may determine the current map date for each FIRM panel by visiting the FEMA Flood Map Service Center website or by calling the FEMA Map Information eXchange.

Communities annexing land on adjacent FIRM panels must obtain a current copy of the adjacent panel as well as the current FIRM Index. These may be ordered directly from the Flood Map Service Center at the number listed above.

For community and countywide map dates, refer to Table 28 in this FIS Report.

To determine if flood insurance is available in the community, contact your insurance agent or call the National Flood Insurance Program at 1-800-638-6620.

The map is for use in administering the NFIP. It may not identify all areas subject to flooding, particularly from local drainage sources of small size. Consult the community map repository to find updated or additional flood hazard information.

<u>BASE FLOOD ELEVATIONS</u>: For more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables within this FIS Report. Use the flood elevation data within the FIS Report in conjunction with the FIRM for construction and/or floodplain management.

Coastal Base Flood Elevations shown on the map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Coastal flood elevations are also provided in the Coastal Transect Parameters table in the FIS Report for this jurisdiction. Elevations shown in the Coastal Transect Parameters table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on the FIRM.

<u>FLOODWAY INFORMATION</u>: Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the FIS Report for this jurisdiction.

#### Figure 2. FIRM Notes to Users

<u>FLOOD CONTROL STRUCTURE INFORMATION</u>: Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 4.3 "Non-Levee Flood Protection Measures" of this FIS Report for information on flood control structures for this jurisdiction.

<u>PROJECTION INFORMATION</u>: The projection used in the preparation of the map was Universal Transverse Mercator (UTM) Zone 10N. The horizontal datum was NAD83, GRS1980 spheroid. Differences in datum, spheroid, projection or State Plane zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of the FIRM.

<u>ELEVATION DATUM</u>: Flood elevations on the FIRM are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at www.ngs.noaa.gov/ or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 (301) 713-3242

Local vertical monuments may have been used to create the map. To obtain current monument information, please contact the appropriate local community listed in Table 31 of this FIS Report.

<u>BASE MAP INFORMATION</u>: Base map information shown on the FIRM was derived from Coastal California LiDAR and digital imagery dated 2011. USDA NAIP imagery dated 2014 is used in areas not covered by the Coastal California digital imagery. For information about base maps, refer to Section 6.2 "Base Map" in this FIS Report.

Corporate limits shown on the map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after the map was published, map users should contact appropriate community officials to verify current corporate limit locations.

#### Figure 2. FIRM Notes to Users

#### NOTES FOR FIRM INDEX

<u>REVISIONS TO INDEX</u>: As new studies are performed and FIRM panels are updated within Santa Cruz County, California, corresponding revisions to the FIRM Index will be incorporated within the FIS Report to reflect the effective dates of those panels. Please refer to Table 28 of this FIS Report to determine the most recent FIRM revision date for each community. The most recent FIRM panel effective date will correspond to the most recent index date.

#### SPECIAL NOTES FOR SPECIFIC FIRM PANELS

This Notes to Users section was created specifically for Santa Cruz County, California, effective September 29, 2017.

<u>ACCREDITED LEVEE</u>: Check with your local community to obtain more information, such as the estimated level of protection provided (which may exceed the 1-percent-annual-chance level) and Emergency Action Plan, on the levee system(s) shown as providing protection for areas on this panel. To mitigate flood risk in residual risk areas, property owners and residents are encouraged to consider flood insurance and floodproofing or other protective measures. For more information on flood insurance, interested parties should visit www.fema.gov/national-flood-insurance-program.

<u>FLOOD RISK REPORT</u>: A Flood Risk Report (FRR) may be available for many of the flooding sources and communities referenced in this FIS Report. The FRR is provided to increase public awareness of flood risk by helping communities identify the areas within their jurisdictions that have the greatest risks. Although non-regulatory, the information provided within the FRR can assist communities in assessing and evaluating mitigation opportunities to reduce these risks. It can also be used by communities developing or updating flood risk mitigation plans. These plans allow communities to identify and evaluate opportunities to reduce potential loss of life and property. However, the FRR is not intended to be the final authoritative source of all flood risk data for a project area; rather, it should be used with other data sources to paint a comprehensive picture of flood risk.

Each FIRM panel contains an abbreviated legend for the features shown on the maps. However, the FIRM panel does not contain enough space to show the legend for all map features. Figure 3 shows the full legend of all map features. Note that not all of these features may appear on the FIRM panels in Santa Cruz County.

#### Figure 3: Map Legend for FIRM

**SPECIAL FLOOD HAZARD AREAS:** The 1% annual chance flood, also known as the base flood or 100-year flood, has a 1% chance of happening or being exceeded each year. Special Flood Hazard Areas are subject to flooding by the 1% annual chance flood. The Base Flood Elevation is the water surface elevation of the 1% annual chance flood. The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. See note for specific types. If the floodway is too narrow to be shown, a note is shown.

Special Flood Hazard Areas subject to inundation by the 1% annual chance flood (Zones A, AE, AH, AO, AR, A99, V and VE)

- Zone A The flood insurance rate zone that corresponds to the 1% annual chance floodplains. No base (1% annual chance) flood elevations (BFEs) or depths are shown within this zone.
- Zone AE The flood insurance rate zone that corresponds to the 1% annual chance floodplains. Base flood elevations derived from the hydraulic analyses are shown within this zone, either at cross section locations or as static whole-foot elevations that apply throughout the zone.
- Zone AH The flood insurance rate zone that corresponds to the areas of 1% annual chance shallow flooding (usually areas of ponding) where average depths are between 1 and 3 feet. Whole-foot BFEs derived from the hydraulic analyses are shown at selected intervals within this zone.
- Zone AO The flood insurance rate zone that corresponds to the areas of 1% annual chance shallow flooding (usually sheet flow on sloping terrain) where average depths are between 1 and 3 feet. Average whole-foot depths derived from the hydraulic analyses are shown within this zone.
- Zone AR The flood insurance rate zone that corresponds to areas that were formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.
- Zone A99 The flood insurance rate zone that corresponds to areas of the 1% annual chance floodplain that will be protected by a Federal flood protection system where construction has reached specified statutory milestones. No base flood elevations or flood depths are shown within this zone.
  - Zone V The flood insurance rate zone that corresponds to the 1% annual chance coastal floodplains that have additional hazards associated with storm waves. Base flood elevations are not shown within this zone.
- Zone VE Zone VE is the flood insurance rate zone that corresponds to the 1% annual chance coastal floodplains that have additional hazards associated with storm waves. Base flood elevations derived from the coastal analyses are shown within this zone as static whole-foot elevations that apply throughout the zone.

### Figure 3: Map Legend for FIRM

	Regulatory Floodway determined in Zone AE.
OTHER AREAS OF FLOO	D HAZARD
	Shaded Zone X: Areas of 0.2% annual chance flood hazards and areas of 1% annual chance flood hazards with average depths of less than 1 foot or with drainage areas less than 1 square mile.
	Future Conditions 1% Annual Chance Flood Hazard – Zone X: The flood insurance rate zone that corresponds to the 1% annual chance floodplains that are determined based on future-conditions hydrology. No base flood elevations or flood depths are shown within this zone.
	Area with Reduced Flood Risk due to Levee: Areas where an accredited levee, dike, or other flood control structure has reduced the flood risk from the 1% annual chance flood. See Notes to Users for important information.
OTHER AREAS	
	Zone D (Areas of Undetermined Flood Hazard): The flood insurance rate zone that corresponds to unstudied areas where flood hazards are undetermined, but possible.
NO SCREEN	Unshaded Zone X: Areas of minimal flood hazard.
FLOOD HAZARD AND OT	HER BOUNDARY LINES
(ortho) (vector)	Flood Zone Boundary (white line on ortho-photography-based mapping; gray line on vector-based mapping)
	Limit of Study
	Jurisdiction Boundary
	Limit of Moderate Wave Action (LiMWA): Indicates the inland limit of the area affected by waves greater than 1.5 feet
GENERAL STRUCTURES	
Aqueduct Channel Culvert Storm Sewer	Channel, Culvert, Aqueduct, or Storm Sewer
Dam Jetty Weir	Dam, Jetty, Weir



#### Figure 3: Map Legend for FIRM

ZONE AO (DEPTH 2)	Zone designation with Depth
ZONE AO (DEPTH 2) (VEL 15 FPS)	Zone designation with Depth and Velocity
BASE MAP FEATURES	
Missouri Creek	River, Stream or Other Hydrographic Feature
(234)	Interstate Highway
234	U.S. Highway
(234)	State Highway
234	County Highway
MAPLE LANE	Street, Road, Avenue Name, or Private Drive if shown on Flood Profile
RAILROAD	Railroad
	Horizontal Reference Grid Line
	Horizontal Reference Grid Ticks
+	Secondary Grid Crosshairs
Land Grant	Name of Land Grant
7	Section Number
R. 43 W. T. 22 N.	Range, Township Number
<sup>42</sup> 76 <sup>000m</sup> E	Horizontal Reference Grid Coordinates (UTM)
365000 FT	Horizontal Reference Grid Coordinates (State Plane)
80° 16' 52.5"	Corner Coordinates (Latitude, Longitude)

### Figure 3: Map Legend for FIRM

#### **SECTION 2.0 – FLOODPLAIN MANAGEMENT APPLICATIONS**

#### 2.1 Floodplain Boundaries

To provide a national standard without regional discrimination, the 1% annual chance (100-year) flood has been adopted by FEMA as the base flood for floodplain management purposes. The 0.2% annual chance (500-year) flood is employed to indicate additional areas of flood hazard in the community.

Each flooding source included in the project scope has been studied and mapped using professional engineering and mapping methodologies that were agreed upon by FEMA and Santa Cruz County as appropriate to the risk level. Flood risk is evaluated based on factors such as known flood hazards and projected impact on the built environment. Engineering analyses were performed for each studied flooding source to calculate its 1% annual chance flood elevations; elevations corresponding to other floods (e.g. 10-, 4-, 2-, 0.2-percent annual chance, etc.) may have also been computed for certain flooding sources. Engineering models and methods are described in detail in Section 5.0 of this FIS Report. The modeled elevations at cross sections were used to delineate the floodplain boundaries on the FIRM; between cross sections, the boundaries were interpolated using elevation data from various sources. More information on specific mapping methods is provided in Section 6.0 of this FIS Report.

Depending on the accuracy of available topographic data (Table 23), study methodologies employed (Section 5.0), and flood risk, certain flooding sources may be mapped to show both the 1% and 0.2% annual chance floodplain boundaries, regulatory water surface elevations (BFEs), and/or a regulatory floodway. Similarly, other flooding sources may be mapped to show only the 1% annual chance floodplain boundary on the FIRM, without published water surface elevations. In cases where the 1% and 0.2% annual chance floodplain boundary is shown on the FIRM. Figure 3, "Map Legend for FIRM", describes the flood zones that are used on the FIRMs to account for the varying levels of flood risk that exist along flooding sources within the project area. Table 2 and Table 3 indicate the flood zone designations for each flooding source and each community within Santa Cruz County, California, respectively.

Table 2, "Flooding Sources Included in this FIS Report," lists each flooding source, including its study limits, affected communities, mapped zone on the FIRM, and the completion date of its engineering analysis from which the flood elevations on the FIRM and in the FIS Report were derived. Descriptions and dates for the latest hydrologic and hydraulic analyses of the flooding sources are shown in Table 13. Floodplain boundaries for these flooding sources are shown on the FIRM (published separately) using the symbology described in Figure 3. On the map, the 1% annual chance floodplain corresponds to the SFHAs. The 0.2% annual chance floodplain shows areas that, although out of the regulatory floodplain, are still subject to flood hazards.

Small areas within the floodplain boundaries may lie above the flood elevations but cannot be shown due to limitations of the map scale and/or lack of detailed topographic data. The procedures to remove these areas from the SFHA are described in Section 6.5 of this FIS Report.

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Aptos Creek	Santa Cruz County, Unincorporated Areas	Approximately 60 feet upstream of the confluence with the Pacific Ocean	Approximately 0.8 mile upstream of Soquel Drive	18060015	1.5		Y	A, AE	
Arana Gulch	Santa Cruz County, Unincorporated Areas	Approximately 3,000 feet downstream of Capitola Road	Approximately 100 feet upstream of Brookwood Drive	18060015	1.3		Y	AE	1983
Baldwin Creek	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	At Coast Road	18050006	0.3		N	A	1983
Bean Creek	Santa Cruz County, Unincorporated Areas; Scotts Valley, City of	Confluence with Zayante Creek	Approximately 87 feet upstream of Bean Creek Road	18060015	4.2		N	A	1983
Bear Creek	Santa Cruz County, Unincorporated Areas	Confluence with San Lorenzo River	Approximately 3,400 feet upstream of Amber Ridge Loop	18060015	4.4		N	A	1983
Boulder Creek	Santa Cruz County, Unincorporated Areas	Confluence with San Lorenzo River	Approximately 2,720 feet upstream of Big Basin Highway	18060015	5.0		N	A	1983

#### Table 2: Flooding Sources Included in this FIS Report

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Branciforte Creek	Santa Cruz, City of; Santa Cruz County, Unincorporated Areas	Confluence with San Lorenzo River	Approximately 530 feet upstream of Wild Flower Lane	18060015	7.4	<u></u>	N	A, AE	1983
Browns Creek	Santa Cruz County, Unincorporated Areas	Confluence with Corralitos Creek	Approximately 1,950 feet upstream of Via del Sol	18060002	0.7		N	A	1983
Carbonera Creek	Scotts Valley, City of	Confluence with Branciforte Creek	Approximately 50 feet upstream of Carbonera Drive	18060015	1.2		Y	AE	1982
Carbonera Creek	Scotts Valley, City of	Approximately 50 feet upstream of Carbonera Drive	Approximately 1.5 miles upstream of State Highway 17	18060015	5.9		Y	A, AE	1982
College Lake	Santa Cruz County, Unincorporated Areas	Confluence with Corralitos Creek	Approximately 2,600 feet upstream of Paulsen Road	18060002	0.9		N	AE	1983
Corralitos Creek	Santa Cruz County, Unincorporated Areas	Lake Avenue	Approximately 355 feet upstream of confluence of Mormon Gulch	18060002	8.9		Y	A, AE	1983
Coward Creek	Santa Cruz County, Unincorporated Areas	Confluence with the Pajaro River	Approximately 4,450 feet upstream of Riverside Road	18060002	1.0		Ν	AE	1983
Drew Lake	Santa Cruz County, Unincorporated Areas	At College Road	Approximately 3,320 feet upstream of College Road	18060002		0.015	N	A	1983

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Gallighan Slough	Santa Cruz County, Unincorporated Areas	Confluence with Harkins Slough	Approximately 0.5 mile upstream of confluence with Harkins Slough	18060002	0.5		Ν	A	1983
Hanson Slough	Santa Cruz County, Unincorporated Areas	Confluence with Watsonville Slough	Approximately 1 mile upstream of confluence with Watsonville Slough	18060002	1.1		N	A	1983
Hare Creek	Santa Cruz County, Unincorporated Areas	Confluence with Boulder Creek	Approximately 0.6 mile upstream of confluence with Boulder Creek	18060015	0.6		Ν	A	1983
Harkins Slough	Santa Cruz County, Unincorporated Areas	Confluence with Watsonville Slough	Approximately 0.7 mile upstream of Dunlap Lane	18060002	6.3		Y	A, AE	1983
Hopkins Gulch	Santa Cruz County, Unincorporated Areas	Confluence with Bear Creek	Approximately 23 feet upstream of Wicket Road	18060015	0.3		N	A	1983
Kelly Lake	Santa Cruz County, Unincorporated Areas	At College Road	Approximately 4,020 feet upstream of College Road	18060002		0.07	N	A	1983
Kings Creek	Santa Cruz County, Unincorporated Areas	Confluence with San Lorenzo River	Approximately 0.7 mile upstream of Highway 9	18060015	0.8		N	A	1983

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Laguna Creek	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	Approximately 3,040 feet upstream of confluence with Pacific Ocean	18060006	0.6		N	A	1983
Lake Tynan	Santa Cruz County, Unincorporated Areas	Approximately 4,500 feet upstream of Riverside Road	Approximately 900 feet downstream of Lakeview Road	18060002	0.4		N	AE	1983
Loch Lomond Reservoir	Santa Cruz County, Unincorporated Areas	Approximately 200 feet upstream of Newell Creek Road	Approximately 2.4 miles upstream of Newell Creek Road	18060015	0.2		N	A	1983
Lompico Creek	Santa Cruz County, Unincorporated Areas	At mouth	Approximately 2.7 miles upstream from mouth	18060015	2.7		N	A	2011
Love Creek	Santa Cruz County, Unincorporated Areas	Approximately 900 feet upstream of Brookside Avenue	Approximately 1,560 feet upstream of Love Creek Road	18060015	1.6		N	A	1983
Majors Creek	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	Approximately 780 feet upstream of State Highway 1	18060006	0.6		N	A	1983
Mill Creek	Santa Cruz County, Unincorporated Areas	Confluence with Scott Creek	Approximately 880 feet upstream of Swanton Road	18060006	0.3		N	A	1983

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Molino Creek	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	Approximately 0.6 mile upstream of Swanton Road	18060006	1.0		N	A	1983
Moore Creek	Santa Cruz County, Unincorporated Areas	Confluence with the Pacific Ocean	At Meder Street	18060015	2.4		Y	A, AE	1983
Moran Lake	Santa Cruz County, Unincorporated Areas	At East Cliff Drive	Approximately 1,447 feet upstream of East Cliff Drive	18060015	0.3		N	A	1983
Newell Creek	Santa Cruz County, Unincorporated Areas	Confluence with San Lorenzo River	At Loch Lomond Reservoir	18060015	1.8		N	A	1983
Nobel Creek	Capitola, City of	Confluence with Soquel Creek	At Kennedy Drive	18060015	0.9		Y	AE	1983
Old Dairy Gulch	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	Approximately 1,775 feet upstream of Union Pacific Railroad	18060006	0.7		N	A	1983
Pacific Ocean	Santa Cruz County, Unincorporated Areas	North Monterey County border	South San Mateo County Border	18060002 18060006 18060015	38.4		N	AE, VE	2013

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Pajaro River	Santa Cruz County, Unincorporated Areas; Watsonville, City of	Approximately 800 feet downstream of the confluence with Watsonville Slough	Approximately 0.8 mile upstream of Riverside Drive	18060002	19.4		Y	A, AE	1983
Pinto Lake	Santa Cruz County, Unincorporated Areas; Watsonville, City of	Approximately 1,088 feet upstream of Green Valley Road	Approximately 1 mile upstream of Green Valley Road	18060002		0.2	Ν	A	1983
Rodeo Creek Gulch	Santa Cruz County, Unincorporated Areas	East Cliff Drive	Approximately 1,600 feet upstream of Soquel Drive	18060015	2.6		Y	AE	1983
Rose Reservoir	Santa Cruz County, Unincorporated Areas	Approximately 730 feet upstream of Casserly Road	Approximately 1,390 feet upstream of Casserly Road	18060002	0.1		N	A	1983
Salsipuedes Creek	Santa Cruz County, Unincorporated Areas; Watsonville, City of	Confluence with the Pajaro River	College Lake Outlet	18060002	2.5		N	AE	2009
San Lorenzo River	Santa Cruz, City of; Santa Cruz County, Unincorporated Areas	Confluence with the Pacific Ocean	Approximately 215 feet upstream of Highway 9	18060015	27.1		Y	A, AE	1983

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
San Vicente Creek	Santa Cruz County, Unincorporated Areas	Confluence with the Pacific Ocean	Approximately 1 mile upstream of State Highway 1	18050006	1.0		Y	A, AE	1983
Schwans Lagoon	Santa Cruz County, Unincorporated Areas	Approximately 350 feet downstream of East Cliff Drive	Approximately 1,700 feet upstream of East Cliff Drive	18060015	0.4		N	AE	1983
Scott Creek	Santa Cruz County, Unincorporated Areas	At Coast Road	Approximately 2,835 feet upstream of Purdy Ranch Road	18050006	5.5		N	A	1983
Soquel Creek	Capitola, City of; Santa Cruz County, Unincorporated Areas	Approximately 500 feet downstream of Stockton Avenue	Approximately 2 miles upstream of Hinckley Basin Road	18060015	11.5		Y	A, AE	1983
Struve Slough	Santa Cruz County, Unincorporated Areas; Watsonville, City of	Confluence with Watsonville Slough	Near the concrete culvert outlet at South Green Valley Road	18060002	2.5		Y	AE	2009
Thomasello Creek	Santa Cruz County, Unincorporated Areas	Approximately 1,000 feet upstream of the confluence with the Pajaro River	Approximately 1,000 feet upstream of State Highway 129	18060002	0.8		N	AE	1983
Thompson Creek	Santa Cruz County, Unincorporated Areas	Confluence with the Pajaro River	Approximately 3,800 feet upstream of Carlton Road	18060002	2.1		N	AE	1983

Flooding Source	Community	Downstream Limit	Upstream Limit	HUC-8 Sub- Basin(s)	Length (mi) (streams or coastlines)	Area (mi <sup>2</sup> ) (estuaries or ponding)	Floodway (Y/N)	Zone shown on FIRM	Date of Analysis
Two Bar Creek	Santa Cruz County, Unincorporated Areas	Confluence with San Lorenzo River	Approximately 0.6 mile upstream of Highway 9	18060015	0.6		N	A	1983
Waddell Creek	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	Approximately 2.8 miles upstream of Coast Road	18060006	2.9		N	A	1983
Watsonville Slough	Santa Cruz County, Unincorporated Areas; Watsonville, City of	Confluence with the Pajaro River	Northwest corner of Watsonville Pioneer Cemetery	18060002	6.7		Y	AE	2009
West Branch Struve Slough	Santa Cruz County, Unincorporated Areas; Watsonville, City of	Confluence with Struve Slough	Approximately 1,460 feet upstream of Harkins Slough Road	18060002	0.9		N	A	1983
Wilder Creek	Santa Cruz County, Unincorporated Areas	Confluence with Pacific Ocean	Approximately 1,720 feet upstream of Coast Road	18060006	1.4		N	A	1983
Zayante Creek	Santa Cruz County, Unincorporated Areas	Confluence with the San Lorenzo River	Approximately 2,066 feet upstream of East Zayante Road	18060015	5.9		Y	A, AE	1983

#### 2.2 Floodways

Encroachment on floodplains, such as structures and fill, reduces flood-carrying capacity, increases flood heights and velocities, and increases flood hazards in areas beyond the encroachment itself. One aspect of floodplain management involves balancing the economic gain from floodplain development against the resulting increase in flood hazard.

For purposes of the NFIP, a floodway is used as a tool to assist local communities in balancing floodplain development against increasing flood hazard. With this approach, the area of the 1% annual chance floodplain on a river is divided into a floodway and a floodway fringe based on hydraulic modeling. The floodway is the channel of a stream, plus any adjacent floodplain areas, that must be kept free of encroachment in order to carry the 1% annual chance flood. The floodway fringe is the area between the floodway and the 1% annual chance floodplain boundaries where encroachment is permitted. The floodway must be wide enough so that the floodway fringe could be completely obstructed without increasing the water surface elevation of the 1% annual chance flood more than 1 foot at any point. Typical relationships between the floodway and the floodway fringe and their significance to floodplain development are shown in Figure 4.

To participate in the NFIP, Federal regulations require communities to limit increases caused by encroachment to 1.0 foot, provided that hazardous velocities are not produced. The floodways in this project are presented to local agencies as minimum standards that can be adopted directly or that can be used as a basis for additional floodway projects.



#### Figure 4: Floodway Schematic

Floodway widths presented in this FIS Report and on the FIRM were computed at cross sections. Between cross sections, the floodway boundaries were interpolated. For certain stream segments, floodways were adjusted so that the amount of floodwaters conveyed on each side of the floodplain would be reduced equally. The results of the floodway computations have been tabulated for selected cross sections and are shown in Table 24, "Floodway Data."

All floodways that were developed for this Flood Risk Project are shown on the FIRM using the symbology described in Figure 3. In cases where the floodway and 1% annual chance floodplain boundaries are either close together or collinear, only the floodway boundary has been shown on the FIRM. For information about the delineation of floodways on the FIRM, refer to Section 6.3.

#### 2.3 Base Flood Elevations

The hydraulic characteristics of flooding sources were analyzed to provide estimates of the elevations of floods of the selected recurrence intervals. The Base Flood Elevation (BFE) is the elevation of the 1% annual chance flood. These BFEs are most commonly rounded to the whole foot, as shown on the FIRM, but in certain circumstances or locations they may be rounded to 0.1 foot. Cross section lines shown on the FIRM may also be labeled with the BFE rounded to 0.1 foot. Whole-foot BFEs derived from engineering analyses that apply to coastal areas, areas of ponding, or other static areas with little elevation change may also be shown at selected intervals on the FIRM.

Cross sections with BFEs shown on the FIRM correspond to the cross sections shown in the Floodway Data table and Flood Profiles in this FIS Report. BFEs are primarily intended for flood insurance rating purposes. For construction and/or floodplain management purposes, users are cautioned to use the flood elevation data presented in this FIS Report in conjunction with the data shown on the FIRM.

#### 2.4 Non-Encroachment Zones

This section is not applicable to this Flood Risk Project.

#### 2.5 Coastal Flood Hazard Areas

For most areas along rivers, streams, and small lakes, BFEs and floodplain boundaries are based on the amount of water expected to enter the area during a 1% annual chance flood and the geometry of the floodplain. Floods in these areas are typically caused by storm events. However, for areas on or near ocean coasts, large rivers, or large bodies of water, BFE and floodplain boundaries may need to be based on additional components, including storm surges and waves. Communities on or near ocean coasts face flood hazards caused by offshore seismic events as well as storm events.

Coastal flooding sources that are included in this Flood Risk Project are shown in Table 2.

#### 2.5.1 Water Elevations and the Effects of Waves

Specific terminology is used in coastal analyses to indicate which components have been included in evaluating flood hazards.

The stillwater elevation (SWEL or still water level) is the surface of the water resulting from astronomical tides, storm surge, and freshwater inputs, but excluding wave setup contribution or the effects of waves.

- *Astronomical tides* are periodic rises and falls in large bodies of water caused by the rotation of the earth and by the gravitational forces exerted by the earth, moon and sun.
- *Storm surge* is the additional water depth that occurs during large storm events. These events can bring air pressure changes and strong winds that force water up against the shore.
- *Freshwater inputs* include rainfall that falls directly on the body of water, runoff from surfaces and overland flow, and inputs from rivers.

The 1% annual chance stillwater elevation is the stillwater elevation that has been calculated for a storm surge from a 1% annual chance storm. The 1% annual chance storm surge can be determined from analyses of tidal gage records, statistical study of regional historical storms, or other modeling approaches. Stillwater elevations for storms of other frequencies can be developed using similar approaches.

The total stillwater elevation (also referred to as the mean water level) is the stillwater elevation plus wave setup contribution but excluding the effects of waves.

• *Wave setup* is the increase in stillwater elevation at the shoreline caused by the reduction of waves in shallow water. It occurs as breaking wave momentum is transferred to the water column.

Like the stillwater elevation, the total stillwater elevation is based on a storm of a particular frequency, such as the 1% annual chance storm. Wave setup is typically estimated using standard engineering practices or calculated using models, since tidal gages are often sited in areas sheltered from wave action and do not capture this information.

Coastal analyses may examine the effects of overland waves by analyzing storm-induced erosion, overland wave propagation, wave runup, and/or wave overtopping.

- *Storm-induced erosion* is the modification of existing topography by erosion caused by a specific storm event, as opposed to general erosion that occurs at a more constant rate.
- *Overland wave propagation* describes the combined effects of variation in ground elevation, vegetation, and physical features on wave characteristics as waves move onshore.
- *Wave runup* is the uprush of water from wave action on a shore barrier. It is a function of the roughness and geometry of the shoreline at the point where the stillwater elevation intersects the land.
- *Wave overtopping* refers to wave runup that occurs when waves pass over the crest of a barrier.



#### Figure 5: Wave Runup Transect Schematic

#### 2.5.2 Floodplain Boundaries and BFEs for Coastal Areas

For coastal communities along the Atlantic and Pacific Oceans, the Gulf of Mexico, the Great Lakes, and the Caribbean Sea, flood hazards must take into account how storm surges, waves, and extreme tides interact with factors such as topography and vegetation. Storm surge and waves must also be considered in assessing flood risk for certain communities on rivers or large inland bodies of water.

Beyond areas that are affected by waves and tides, coastal communities can also have riverine floodplains with designated floodways, as described in previous sections.

#### **Floodplain Boundaries**

In many coastal areas, storm surge is the principle component of flooding. The extent of the 1% annual chance floodplain in these areas is derived from the total stillwater elevation (stillwater elevation including storm surge plus wave setup) for the 1% annual chance storm. The methods that were used for calculation of total stillwater elevations for coastal areas are described in Section 5.3 of this FIS Report. Location of total stillwater elevations for coastal areas are shown in Figure 8, "1% Annual Chance Total Stillwater Levels for Coastal Areas."

In some areas, the 1% annual chance floodplain is determined based on the limit of wave runup or wave overtopping for the 1% annual chance storm surge. The methods that were used for calculation of wave hazards are described in Section 5.3 of this FIS Report.

Table 26 presents the types of coastal analyses that were used in mapping the 1% annual chance floodplain in coastal areas.

#### **Coastal BFEs**

Coastal BFEs are calculated as the total stillwater elevation (stillwater elevation including storm surge plus wave setup) for the 1% annual chance storm plus the additional flood hazard from overland wave effects (storm-induced erosion, overland wave propagation, wave runup and wave overtopping).

Where they apply, coastal BFEs are calculated along transects extending from offshore to the limit of coastal flooding onshore. Results of these analyses are accurate until local topography, vegetation, or development type and density within the community undergoes major changes.

Parameters that were included in calculating coastal BFEs for each transect included in this FIS Report are presented in Table 17, "Coastal Transect Parameters." The locations of transects are shown in Figure 9, "Transect Location Map." More detailed information about the methods used in coastal analyses and the results of intermediate steps in the coastal analyses are presented in Section 5.3 of this FIS Report. Additional information on specific mapping methods is provided in Section 6.4 of this FIS Report.

#### 2.5.3 Coastal High Hazard Areas

Certain areas along the open coast and other areas may have higher risk of experiencing structural damage caused by wave action and/or high-velocity water during the 1% annual chance flood. These areas will be identified on the FIRM as Coastal High Hazard Areas.

- *Coastal High Hazard Area (CHHA)* is a SFHA extending from offshore to the inland limit of the primary frontal dune (PFD) or any other area subject to damages caused by wave action and/or high-velocity water during the 1% annual chance flood.
- *Primary Frontal Dune (PFD)* is a continuous or nearly continuous mound or ridge of sand with relatively steep slopes immediately landward and adjacent to the beach. The PFD is subject to erosion and overtopping from high tides and waves during major coastal storms.

CHHAs are designated as "V" zones (for "velocity wave zones") and are subject to more stringent regulatory requirements and a different flood insurance rate structure. The areas of greatest risk are shown as VE on the FIRM. Zone VE is further subdivided into elevation zones and shown with BFEs on the FIRM.

The landward limit of the PFD occurs at a point where there is a distinct change from a relatively steep slope to a relatively mild slope; this point represents the landward extension of Zone VE. Areas of lower risk in the CHHA are designated with Zone V on the FIRM. More detailed information about the identification and designation of Zone VE is presented in Section 6.4 of this FIS Report.

Areas that are not within the CHHA but are SFHAs may still be impacted by coastal flooding and damaging waves; these areas are shown as "A" zones on the FIRM.

Figure 6, "Coastal Transect Schematic," illustrates the relationship between the base flood elevation, the 1% annual chance stillwater elevation, and the ground profile as well as the location of the Zone VE and Zone AE areas in an area without a PFD subject to overland wave propagation. This figure also illustrates energy dissipation and regeneration of a wave as it moves inland.



#### **Figure 6: Coastal Transect Schematic**

Methods used in coastal analyses in this Flood Risk Project are presented in Section 5.3 and mapping methods are provided in Section 6.4 of this FIS Report.

Coastal floodplains are shown on the FIRM using the symbology described in Figure 3, "Map Legend for FIRM." In many cases, the BFE on the FIRM is higher than the stillwater elevations shown in Table 17 due to the presence of wave effects. The higher elevation should be used for construction and/or floodplain management purposes.

#### 2.5.4 Limit of Moderate Wave Action

This section is not applicable to this Flood Risk Project.

#### **SECTION 3.0 – INSURANCE APPLICATIONS**

#### 3.1 National Flood Insurance Program Insurance Zones

For flood insurance applications, the FIRM designates flood insurance rate zones as described in Figure 3, "Map Legend for FIRM." Flood insurance zone designations are assigned to flooding sources based on the results of the hydraulic or coastal analyses. Insurance agents use the zones shown on the FIRM and depths and base flood elevations in this FIS Report in conjunction with information on structures and their contents to assign premium rates for flood insurance policies.

The 1% annual chance floodplain boundary corresponds to the boundary of the areas of special flood hazards (e.g. Zones A, AE, V, VE, etc.), and the 0.2% annual chance floodplain boundary corresponds to the boundary of areas of additional flood hazards.

Table 3 lists the flood insurance zones in Santa Cruz County.
Community	Flood Zone(s)
Capitola, City of	AE, VE, X
Santa Cruz, City of	A, AE, A99, VE, X
Santa Cruz County, Unincorporated Areas	A, AE, AH, AO, VE, X
Scotts Valley, City of	A, AE, X
Watsonville, City of	A, AE, AH, AO, X

### Table 3: Flood Zone Designations by Community

### 3.2 Coastal Barrier Resources System

This section is not applicable to this Flood Risk Project.

#### Table 4: Coastal Barrier Resources System Information

#### [Not Applicable to this Flood Risk Project]

## **SECTION 4.0 – AREA STUDIED**

#### 4.1 Basin Description

Table 5 contains a description of the characteristics of the HUC-8 sub-basins within which each community falls. The table includes the main flooding sources within each basin, a brief description of the basin, and its drainage area.

HUC-8 Sub- Basin Name	HUC-8 Sub-Basin Number	Primary Flooding Source	Description of Affected Area	Drainage Area (square miles)
Pajaro	18060002	Pajaro River	Drainage basin encompasses an area including the major communities of the City of Watsonville, and the Towns of Corralitos, Freedom, Pajaro, and Watsonville Junction. The Pajaro River, the principal stream in the Pajaro Valley, flows along the southeastern edge of the City of Watsonville.	1,300
San Francisco Coastal South	18050006	Pacific Ocean	*	*

**Table 5: Basin Characteristics** 

HUC-8 Sub- Basin Name	HUC-8 Sub-Basin Number	Primary Flooding Source	Description of Affected Area	Drainage Area (square miles)
Monterey Bay	18060015	San Lorenzo River	The largest basin contained within the county is the San Lorenzo River basin which begins at the confluence of Monterey Bay at the Pacific Ocean and extends approximately 20 miles north from the river mouth into the coastal mountains.	137

\*Data not available

## 4.2 Principal Flood Problems

Table 6 contains a description of the principal flood problems that have been noted for Santa Cruz County by flooding source.

Flooding Source	Description of Flood Problems
All sources	The wet season in Santa Cruz County generally extends from October through May, but most flooding has occurred from December through March. In all streams except the Pajaro River, flood flow stages can rise from normal flow to extreme flood peaks in a few hours with high velocities in the main channels. Flood peaks at the lower end of the Pajaro River, however, occur approximately 24 hours after the flood-producing rainfall, mainly because of its large drainage area (USACE 1963). Flooding is most severe when antecedent rainfall has produced saturated ground conditions.
	Isoding has occurred in Santa Cruz County at various times throughout the last 100 years. Major storms are known to have occurred during March 1899, December 1937, February 1940, January 1943, November 1950, January 1952, December 1955, April 1958, January 1963, January 1967, and January 1982. The most significant floods occurred in 1955 and 1982 (USACE 1963, USACE 1973(a), USACE 1973(b), USACE 1976).
All Sources Within the City of Watsonville	In the City of Watsonville, storms of flood-producing magnitude occur most often during the months of December through April, although they can occur as early as September and as late as May. Storms occurring early in the rainfall season are unlikely to result in excessive runoff since infiltration and surface-storage capacities are high.
	Some flooding occurred along the southeastern perimeter of Watsonville on January 4, 1982. The flooding resulted from the overflow of Corralitos Creek and produced shallow flooding in a 200- to 1,000-foot-wide strip along Bridge Street and Riverside Drive. Several homes near the eastern end of Tuttle Avenue adjacent to Salsipuedes Creek were damaged because of the ponding of this overflow. No other major damage resulted in Watsonville from this storm.

## Table 6: Principal Flood Problems

Flooding Source	Description of Flood Problems			
	In general, the following three principal flood problems can affect the City of Watsonville:			
	<ol> <li>Inadequate interior drainage can create shallow flooding conditions from the accumulation of surface runoff.</li> </ol>			
	<ol> <li>Flood damage can come from the overtopping of the Salsipuedes Creek or Pajaro River levees. The USACE has indicated that it is reasonable to assume that the Pajaro River levees would fail during a major event, such as the 1- percent-annual-chance flood, when flows significantly exceed the channel capacity. The Salsipuedes Creek levees may remain intact during the 1- percent-annual- chance event because of the limited overflow volume and duration.</li> <li>The overflow of Corralitos Creek upstream of the levees can cause</li> </ol>			
	flooding in the eastern half of the city. Flow which overtops Corralitos Creek is unable to re-enter downstream because of the levees.			
All Sources Within the City of Scotts Valley	In Scotts Valley, significant flooding problems were experienced during the first week of January 1982. In addition, flooding is thought to have occurred in the Scotts Valley area in December 1955; however no detailed information recounting the extent and location of flood damage in 1955 was found. Because there are no gages on the creeks in Scotts Valley, the recurrence interval of these floods could not be estimated. Heavy rain caused flash flooding in January 2008 that closed many roads including Highway 9 and submerged the hardwood gym floor at Scotts Valley High School causing \$300,000 in damage (Commerce 2010).			
	Because the watershed is heavily wooded, other debris problems occurred in the City of Scotts Valley. For example, a log jam occurred at the Glen Canyon Road Bridge at the southern end of the city. In one case, a car was carried into Camp Evers Creek but was removed before it obstructed a bridge.			
All Sources Within the City of Santa Cruz	The City of Santa Cruz was not inundated as it was in 1955 because of the protection afforded by the levees, but damage upstream of the City of Santa Cruz along the San Lorenzo River was extensive. The damage was most extensive in the area between the upstream corporate limits and Felton, and in the Towns of Paradise Park, Gold Gulch, and Felton Grove. In the Felton Grove area, floodwaters in the overbanks reached depths of 3 to 7 feet and inundated 50 homes and cabins. An additional 60 to 70 homes and businesses were flooded between Felton and Ben Lomond.			
Aptos Creek	In the Aptos Creek basin just east of the Soquel basin, only minor damage resulted from the December 1955 storm (USACE 1956). A total of 140 acres of land was inundated by floodwaters, which caused \$62,000 in damage. Four homes along Moosehead Drive experienced flooding, while the Valencia Road crossing was heavily damaged. Other bridges receiving minor damage included the bridge on Aptos Creek, just south of the confluence with Valencia Creek, and the Southern Pacific Railroad (SPRR) Bridge (USACE July 1973 (a.)). Similar flooding was experienced in the Aptos Creek basin during the			
	January 1982 storm. The estimated peak discharge on Aptos Creek on January 3, 1982, was 3,950 cfs, in contrast to the December 1955 peak flow of 3,500 cfs. The 1982 peak flow corresponded to a 2.50-percent-annual-			

Flooding Source	Description of Flood Problems
	chance recurrence interval, as measured at the Aptos gage. Heavy damage resulted from the 1982 storm. At least seven homes along Moosehead and Spreckels Drives between the State Highway 1 and Spreckels Drive bridges suffered major damage (Briggs 1982). Further downstream damage resulted to major portions of two streets paralleling Aptos Creek.
Carbonera Creek	Damage from the January 1982 flood occurred in a number of different locations in Scotts Valley. Significant damage was sustained to a home and to channel banks near the confluence of Camp Evers and Carbonera Creeks. According to city officials, some flooding occurs at this location approximately 3 out of every 10 years. Floodwaters along Carbonera Creek also damaged bridges. Parts of an abandoned bridge on Bob Jones Lane and all of the Carbonera Creek Industrial Park Bridge were washed out. Extensive bank erosion occurred around the El Pueblo Road Bridge, as well as just downstream of the bridge behind a lumberyard. Bank erosion also produced loss of land in various other locations along Carbonera Creek.
	Because the watershed is heavily wooded, other debris problems occurred in the City of Scotts Valley. For example, a log jam occurred at the Glen Canyon Road Bridge at the southern end of the city. In one case, a car was carried into Camp Evers Creek but was removed before it obstructed a bridge.
Corralitos Creek	Significant flooding along Corralitos and Salsipuedes Creeks also occurred in December 1955 and April 1958. Peak discharges for Corralitos Creek at Green Valley Road have been estimated from high-water elevations (USACE 1956). The estimated discharges for the 1955 and 1958 floods are 3,620 cfs and 2,680 cfs, which correspond to 8.33- and 14.29-percent- annual-chance recurrence intervals, respectively. The overflow of Corralitos Creek upstream of the leveed section on Salsipuedes Creek flooded 29 blocks within the City of Watsonville during the December 1955 flood (USACE 1956). The 1-percent-annual-chance discharge for Corralitos Creek at Green Valley is 7,900 cfs.
San Lorenzo River	While the rainy season for the City of Santa Cruz extends from October through May, flooding has occurred primarily in December, January, and February. The City of Santa Cruz has a history of periodic flooding, particularly from the San Lorenzo River. News-papers report early floods in January 1862, January 1869, January 1890, January 1895, January 1909, January 1911, and December 1931 (Santa Cruz County, Office of Watershed 1979). Since the USGS stream gage on the San Lorenzo River was installed at Felton in 1937, damaging floods have been recorded in February 1940, December 1955, April 1958, and January 1982, with peak discharges of 24,000 cfs, 30,400 cfs, 17,200 cfs, and 19,700 cfs, respectively. In the San Lorenzo River basin, a total of \$8.7 million in damages resulted
	trom intense rainfall between December 21 and 24, 1955, with \$7.6 million in damages occurring in the City of Santa Cruz (USACE 1979). Flooding reached depths as high as 6.5 feet on Front Street and inundated 410 acres in the city. Five people in the city were killed and 2,400 people were displaced by the floods. The most extensive damage in the county occurred in the Felton, Ben Lomond, and Boulder Creek areas where over 300 people were displaced or evacuated. At Ben Lomond, the San Lorenzo River remained above its banks for 83 hours. Severe local flooding occurred

Flooding Source	Description of Flood Problems				
	because of logjams that diverted high- velocity flows, damaging bridges, private developments, and other lands. A total of 1,765 acres was flooded and two lives lost in the county portion of the basin. The estimated peak discharge for the San Lorenzo River at the Big Trees gaging station was 30,400 cubic feet per second (cfs) which corresponds to a 3.33-percent- annual-chance recurrence interval.				
	On January 3 and 4, 1982, high flows occurred on the San Lorenzo River. These flows, however, did not cause heavy damage to the City of Santa Cruz due to the construction of a flood-control project in 1958. The estimated flow for the January 1982 storm, 29,700 cfs at the Big Trees gage, was similar to the December 1955 event. These floods each had a 3.33-percent-annual-chance recurrence interval. The levees were not overtopped during the storm, but floodwaters rose to within 3 or 4 feet of the levee tops at peak flow (approximately 35,000 to 37,000 cfs) to downstream of the confluence with Branciforte Creek (Briggs 1982). These high stages occurred even though the estimated flow was considerably lower than the design flow of 53,000 cfs (USACE General Design Memorandum). Branciforte Creek at the confluence with the San Lorenzo River was filled to capacity during the storm.				
	Significant scour occurred in the downtown reach of the San Lorenzo River because of high channel velocities. Scour damaged the Riverside Avenue Bridge and undermined one pier on the Soquel Avenue Bridge, causing on pan to collapse. Cost for bridge repairs was estimated at \$1.75 million (Otto Water Engineers, Inc. 1984). Two cranes worked throughout the flood peak removing logs at bridges, thereby preventing major logjams.				
Soquel Creek	While the rainy season for Soquel Creek generally extends from October through May, the bulk of flooding has occurred in December, January, and February. Floods in the Soquel Creek basin are normally of short duration, lasting approximately 6 to 24 hours. They develop rapidly, with the peak being reached in approximately 4 hours after occurrence of a flood-producing storm.				
	The Soquel Creek basin, particularly the City of Capitola and the Town of Soquel, experienced major flooding in December 1955. In a 72-hour period during December 21- 24, 1955, storm rainfall equivalent to 35 percent of the normal annual precipitation fell on the basin (USACE 1965). A major logjam occurred at the Soquel Avenue Bridge, causing a severe backwater condition. In Soquel, eight city blocks were inundated, displacing 350 persons. Just upstream of the confluence with Hinckley Creek, floodwaters in the overbanks reached depths of 5 to 6 feet. Total damage in the Soquel Creek basin was estimated at \$831,000. The estimated peak flow for Soquel Creek at the Soquel gage was 15,800 cfs, which corresponds to a 1.43-percent-annual-chance recurrence interval. In Capitola, some damage was done to commercial and residential property adjacent to Soquel Creek. The damage resulted from bank erosion and deposition of debris, but the majority of damage caused by the overflow of Soquel Creek occurred outside of Capitola.				
	During the January 1982 flood, the Soquel Creek basin experienced major flooding in the vicinity of the Soquel Avenue Bridge. A massive logjam, which included a four-bedroom house and for auto-court apartments, diverted flow down the main street of the Town of Soquel. The floodwaters				

Flooding Source	Description of Flood Problems				
	rose rapidly along Soquel Creek and caused major damage to two mobile home parks adjacent to the stream. The United States Geological Survey (USGS) estimate for the peak discharge at the Soquel Creek gage was 9,700 cfs, which corresponds to a 6.67-percent-annual-chance recurrence interval.				
	Overflow of Soquel Creek during the January 1982 storm flooded one home on the eastern bank just south of State Highway 1 and eroded the banks of some homes along Riverview Drive in Capitola. According to city officials, however, the most significant damage in Capitola resulted from the flooding of Nobel Creek. The capacity of the long culvert extending from Bay Avenue under the mobile home park and into Soquel Creek was exceeded. Excess flow lifted the manholes in the park and produced shallow flooding conditions. A large portion of this flow passed over Riverview Drive and caused minor damage to about 20 homes south of Riverview before entering Soquel Creek. Other flow traveled south on Capitola Avenue and caused shallow flooding.				
	The Cities of Capitola, Scotts Valley, and Watsonville were also affected by the January 1982 flood. In Capitola, the USGS preliminary estimate of peak flow for Soquel Creek was approximately 9,700 cfs, which is equivalent to 6.67-percent-annual-chance recurrence interval. Although the USGS January 1982 flow estimate at the Soquel gage was 6,100 cfs lower than the December 1955 event, the stage height at the gaging station was only 0.48 foot lower than the maximum height recorded for the 1955 event. The high water surface elevations (WSELs) for the 1982 storm were probably caused by the large logjam that occurred at the Soquel Avenue Bridge just downstream of the gaging station. However, it was noted that a logjam also occurred at the same bridge during the 1955 event. High-water marks downstream at the State Highway 1 Bridge were within 1 foot of each other for the two events (Briggs 1982).				
Pacific Ocean	Flooding along the Pacific coast of Santa Cruz County is typically associated with the simultaneous occurrence of very high tides, large waves, and storm swells during the winter. As a result, ocean-front development has not been compatible with the natural instability of the shoreline and intense winter weather conditions.				
	Tsunamis (sea waves generated from oceanic earthquakes, submarine landslides, and volcanic eruptions) create some of the most destructive natural water waves. As tsunami waves approach shallow coastal waters, wave refraction, shoaling, and bay resonance amplify the wave heights.				
	Storm centers from the southwest produce the type of storm pattern most commonly responsible for the majority of serious coastline flooding. The strong winds and high tides that create storm surges are also accompanied by heavy rains. In some instances, high tides back up riverflows that causes flooding at the river mouths.				
	The most severe storms to hit the California coast occurred in 1978 and 1983 when high- water levels were accompanied by very large storm waves. The most notable events are described below.				
	In January 1978, a series of storms emanated from a more southerly direction than normally occurs; consequently, some of the more protected beaches were also damaged. Storm incidents occurred throughout the				

Flooding Source	Description of Flood Problems				
	study area. Jetties and breakwater barriers were overtopped and in some cases undermined. Direct wave damage occurred to many beachfront homes, especially in the more populated beachfront areas along Monterey Bay. Accelerated erosion coupled with rain and saturated ground conditions weakened the foundations of beach-bluff top homes in Santa Cruz County. Seawalls and temporary barriers failed to protect beachfront properties from the ravages of the 1978 storms.				
	Significant storms and associated damage strike the Monterey Bay communities with a frequency of one large storm every 3 to 4 years. The New Brighton and Seacliff State Beach study areas, as well as the City of Capitola, are directly exposed to storm waves which approach from the west, west-southwest, and southwest across deep waters. The waves undergo little refraction before striking the coastline. Statistics show that 13 out of 20 large storms arrive from the southwest (Otto Water Engineers, Inc. 1984). Repeated damage has occurred to beachfront structures in an area of the coast between the New Brighton State Beach and Seacliff State Beach study sites. Approximately every 7 years, seawalls or bulkheads at Seacliff State Beach are damaged or destroyed. The last episode occurred in 1983 when 3,500 feet of new seawall, a restroom, and 11 recreational vehicle sites were destroyed, which amounts to \$740,000 in damage. In the Seacliff State Beach area, numerous homes have been constructed on fill to raise the height of the backbench. In 1983, an existing protective riprap was overtopped and 19 of 21 homes were significantly damaged. Flooding along the Pacific coast at the Cities of Capitola and Santa Cruz is typically associated with the simultaneous occurrence of very high tides, large waves, and storm swells during the winter. As a result, ocean-front development has not been compatible with the natural instability of the shoreline and the intense winter weather conditions. Much of lower Monterey Bay is bordered by the Pajaro Dunes area, which is a series of older stabilized dunes fronted by younger active dunes. Since 1882, structures which have been constructed in the area (Camp Goodall,				
	1883; 1,700-foot-long wharf, 1911) were partially destroyed by storm waves. Planned lot developments have been subject to rapid beach retreat several times prior to 1968, in 1969, in 1978, and again in 1983 (Otto Water Engineers, Inc. 1984).				
Pajaro River	The Pajaro River experienced flooding events during February 1937, February 1938, March and April 1941, and February 1945, prior to levee construction; also in January 1952, December 1955, and April 1958, upstream of the leveed reaches. An inspection of rainfall records, gaging stations on other streams, and historical accounts indicates flooding also occurred during the years 1852, 1862, 1898, 1908, 1911, 1914, 1917, 1922, and 1932.				
	In the December 1955 flood, and again in April 1958, the Pajaro River was maintained within the levees in the Watsonville area, but the levees were breached 2.1 miles upstream of the confluence with Salsipuedes Creek. Although no lives were lost, 972 people were evacuated and \$1.12 million in damages were incurred. Included in these costs were monies spent to repair levees damaged by erosion. Additional levee repairs were required due to damages caused by the April 1958 flood; however, no other				

Flooding Source	Description of Flood Problems				
	significant damage resulted (USACE 1963).				
	The 1955 and 1958 floods are the two largest on record along the Pajaro River, with associated discharges of 24,000 cfs and 23,500 cfs, respectively, at the Chittenden gage (USACE 1963). The estimated return periods for floods of these magnitudes are 3.70- and 3.85-percent-annual- chance, respectively. In comparison, the estimated discharge at Chittenden for a 1-percent-annual-chance flood is 43,000 cfs.				
West Carbonera Creek	Flooding also occurred along West Branch Carbonera Creek due to the accumulation of siltation and debris. The channel capacity was reduced as siltation clogged the stream just upstream of a drop structure at the confluence with Carbonera Creek. Siltation also blocked the culverts at the Granite Creek Road Interchange.				

Table 7 contains information about historic flood elevations in the communities within Santa Cruz County.

Flooding Source	Location	Historic Peak (Feet NAVD88)	Event Date	Approximate Recurrence Interval (years)	Source of Data
Aptos Creek	Santa Cruz County	*	1982	40	USGS gage
Corralitos Creek	City of Watsonville	*	1958	7	*
Corralitos Creek	Green Valley Road	*	1955	12	*
Pajaro River	Santa Cruz County	*	1958	26	USGS gage
Pajaro River	Santa Cruz County	*	1955	27	USGS gage
San Lorenzo River	City of Santa Cruz	6.5	1955	30	USGS gage
Soquel Creek	City of Capitola	5.52	1982	15	USGS gage
Soquel Creek	City of Capitola and the Town of Soquel	6.0	1955	70	USGS gage

**Table 7: Historic Flooding Elevations** 

\*Data not available

#### 4.3 Non-Levee Flood Protection Measures

Table 8 contains information about non-levee flood protection measures within Santa Cruz County such as dams, jetties, and or dikes. Levees are addressed in Section 4.4 of this FIS Report.

Flooding Source	Structure Name	Type of Measure	Location	Description of Measure
Branciforte Creek	N/A	Channel improvements	From the confluence with the San Lorenzo River at the Soquel Avenue Bridge1 mile upstream	Rectangular concrete channel was constructed
Pacific Ocean	N/A	Jetties	Northern Monterey Bay	Seawalls, boulder-sized riprap, timber, and concrete bulkheads
Pacific Ocean	N/A	Beach Stabilization	Southern Monterey Bay	Revegetation
San Lorenzo River N/A		Channel improvements, and bank protections	Between the SPRR Bridge and the State Highway 1 Bridge	Channel improvements, and bank protections constructed by the USACE
San Lorenzo River	N/A Channel improvements		Upstream of State Highway 1	The modified channel was wider with a lower invert than the natural channel
Soquel Creek	N/A	Bank Protection	Along Soquel Creek	Bank protection works made of various materials, such as riprap, concrete, and timber.

**Table 8: Non-Levee Flood Protection Measures** 

#### 4.4 Levees

For purposes of the NFIP, FEMA only recognizes levee systems that meet, and continue to meet, minimum design, operation, and maintenance standards that are consistent with comprehensive floodplain management criteria. The Code of Federal Regulations, Title 44, Section 65.10 (44 CFR 65.10) describes the information needed for FEMA to determine if a levee system reduces the risk from the 1% annual chance flood. This information must be supplied to FEMA by the community or other party when a flood risk study or restudy is conducted, when FIRMs are revised, or upon FEMA request. FEMA reviews the information for the purpose of establishing the appropriate FIRM flood zone.

Levee systems that are determined to reduce the risk from the 1% annual chance flood are accredited by FEMA. FEMA can also grant provisional accreditation to a levee system that was previously accredited on an effective FIRM and for which FEMA is awaiting data and/or documentation to demonstrate compliance with Section 65.10. These levee systems are referred to as Provisionally Accredited Levees, or PALs. Provisional accreditation provides communities and levee owners with a specified timeframe to obtain the necessary data to confirm the levee's certification status. Accredited levee systems and PALs are shown on the FIRM using the symbology shown in Figure 3 and in Table 9. If the required information for a PAL is not submitted within the required timeframe, or if information indicates that a levee system not longer meets Section 65.10, FEMA will de-accredit the levee system and issue an effective FIRM showing the levee-impacted area as a SFHA.

FEMA coordinates its programs with USACE, who may inspect, maintain, and repair levee systems. The USACE has authority under Public Law 84-99 to supplement local efforts to repair flood control projects that are damaged by floods. Like FEMA, the USACE provides a program to allow public sponsors or operators to address levee system maintenance deficiencies. Failure to do so within the required timeframe results in the levee system being placed in an inactive status in the USACE Rehabilitation and Inspection Program. Levee systems in an inactive status are ineligible for rehabilitation assistance under Public Law 84-99.

FEMA coordinated with the USACE, the local communities, and other organizations to compile a list of levees that exist within Santa Cruz County. Table 9, "Levees," lists all accredited levees, PALs, and de-accredited levees shown on the FIRM for this FIS Report. Other categories of levees may also be included in the table. The Levee ID shown in this table may not match numbers based on other identification systems that were listed in previous FIS Reports. Levees identified as PALs in the table are labeled on the FIRM to indicate their provisional status.

Please note that the information presented in Table 9 is subject to change at any time. For that reason, the latest information regarding any USACE structure presented in the table should be obtained by contacting USACE and accessing the USACE national levee database. For levees owned and/or operated by someone other than the USACE, contact the local community shown in Table 31.

Table 9: L	evees
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Community	Flooding Source	Levee Location	Levee Owner	USACE Levee	Levee ID	Covered Under PL84- 99 Program?	FIRM Panel(s)
Santa Cruz, City of	San Lorenzo River	Left Bank	*	Yes	1901068008	*	06087C0332E
Santa Cruz, City of	San Lorenzo River	Right Bank	*	Yes	1901068010	*	06087C0332E
Santa Cruz, City of	San Lorenzo River	Right Bank	*	Yes	1901068012	*	06087C0332E 06087C0334F
Santa Cruz, City of	San Lorenzo River	Right Bank	*	Yes	1901068016	*	06087C0334F
Santa Cruz, City of	San Lorenzo River	Left Bank	*	Yes	1901068017	*	06087C0332E 06087C0334F
Santa Cruz County, Unincorporated Areas	College Lake	Left Bank	*	*	1901068018	*	06087C0403E
Santa Cruz County, Unincorporated Areas	Pajaro River	Right Bank	*	Yes	1901068001	*	06087C0411E 06087C0412E
Santa Cruz County, Unincorporated Areas	Pajaro River	Right Bank	*	Yes	1901068002	*	06087C0412E
Santa Cruz County, Unincorporated Areas	Pajaro River	Left Bank	*	Yes	1901068003	*	06087C0412E
Santa Cruz County, Unincorporated Areas	Pajaro River	Left Bank	*	Yes	1901068004	*	06087C0412E
Santa Cruz County, Unincorporated Areas	Pajaro River	Right Bank	*	Yes	1901068005	*	06087C0416E 06087C0418E
Santa Cruz County, Unincorporated Areas	Pajaro River	Right Bank	*	Yes	1901068019	*	06087C0456F

Community	Flooding Source	Levee Location	Levee Owner	USACE Levee	Levee ID	Covered Under PL84- 99 Program?	FIRM Panel(s)
Santa Cruz County, Unincorporated Areas; Watsonville, City of	Pajaro River	Right Bank	*	Yes	1901068020	*	06087C0392E 06087C0393E 06087C0394E 06087C0411E 06087C0456F
Santa Cruz County, Unincorporated Areas; Watsonville, City of	Salsipuedes Creek	Right Bank	*	Yes	1901068000	*	06087C0411E
Santa Cruz County, Unincorporated Areas; Watsonville, City of;	Salsipuedes Creek	Right Bank	*	Yes	1901068006	*	06087C0411E
Santa Cruz County, Unincorporated Areas	Salsipuedes Creek	Left Bank	*	Yes	1901068011	*	06087C0411E
Santa Cruz County, Unincorporated Areas; Watsonville, City of	Salsipuedes Creek	Left Bank	*	Yes	1901068021	*	06087C0411E
Santa Cruz County, Unincorporated Areas	Salsipuedes Creek	Left Bank	*	Yes	1901068022	*	06087C0411E
Santa Cruz County, Unincorporated Areas	Soda Lake	Non- Riverine	*	*	1901068030	*	06087C0440E
Santa Cruz County, Unincorporated Areas	Thompson Creek	Right Bank	*	*	1901068033	*	06087C0412E
Santa Cruz County, Unincorporated Areas	Watsonville Slough	Left Bank	*	*	1901068031	*	06087C0452F 06087C0456F
Santa Cruz County, Unincorporated Areas	Watsonville Slough	Left Bank	*	*	1901068032	*	06087C0452F
Watsonville, City of	Salsipuedes Creek	Right Bank	*	Yes	1901068009	*	06087C0411E

\*Data not available

## **SECTION 5.0 – ENGINEERING METHODS**

For the flooding sources in the community, standard hydrologic and hydraulic study methods were used to determine the flood hazard data required for this study. Flood events of a magnitude that are expected to be equaled or exceeded at least once on the average during any 10-, 25-, 50-, 100-, or 500-year period (recurrence interval) have been selected as having special significance for floodplain management and for flood insurance rates. These events, commonly termed the 10-, 25-, 50-, 100-, and 500-year floods, have a 10-, 4-, 2-, 1-, and 0.2% annual chance, respectively, of being equaled or exceeded during any year.

Although the recurrence interval represents the long-term, average period between floods of a specific magnitude, rare floods could occur at short intervals or even within the same year. The risk of experiencing a rare flood increases when periods greater than 1 year are considered. For example, the risk of having a flood that equals or exceeds the 100-year flood (1-percent chance of annual exceedance) during the term of a 30-year mortgage is approximately 26 percent (about 3 in 10); for any 90-year period, the risk increases to approximately 60 percent (6 in 10). The analyses reported herein reflect flooding potentials based on conditions existing in the community at the time of completion of this study. Maps and flood elevations will be amended periodically to reflect future changes.

#### 5.1 Hydrologic Analyses

Hydrologic analyses were carried out to establish the peak elevation-frequency relationships for floods of the selected recurrence intervals for each flooding source studied. Hydrologic analyses are typically performed at the watershed level. Depending on factors such as watershed size and shape, land use and urbanization, and natural or man-made storage, various models or methodologies may be applied. A summary of the hydrologic methods applied to develop the discharges used in the hydraulic analyses for each stream is provided in Table 13. Greater detail (including assumptions, analysis, and results) is available in the archived project documentation.

A summary of the discharges is provided in Table 10. Frequency Discharge-Drainage Area Curves used to develop the hydrologic models may also be shown in Figure 7 for selected flooding sources. A summary of stillwater elevations developed for non-coastal flooding sources is provided in Table 11. (Coastal stillwater elevations are discussed in Section 5.3 and shown in Table 17.) Stream gage information is provided in Table 12.

			Peak Discharge (cfs)						
Flooding Source	Location	Drainage Area (Square Miles)	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance		
Aptos Creek	At mouth	24.5	3,110	*	6,550	8,280	12,700		
Aptos Creek	Above confluence with Valencia Creek	12.4	1,990	*	4,340	5,540	8,670		
Arana Gulch	At mouth	3.3	790	*	1,390	1,650	2,290		
Carbonera Creek	At confluence with Branciforte Creek	7.2	2,250	*	3,680	4,340	5,900		
Carbonera Creek	At southern corporate limits of the City of Scotts Valley	5.2	1,690	*	2,870	3,400	4,750		
Carbonera Creek	Downstream of confluence of West Branch Carbonera Creek	3.0	970	*	1,710	2,070	2,930		
Carbonera Creek	Upstream of confluence with West Branch Carbonera Creek	2.0	700	*	1,230	1,510	2,150		
College Lake	At confluence with Corralitos Creek	20.7	650	*	2,000	2,800	5,500		
Corralitos Creek	East Lake Avenue at junction with Salsipuedes Creek	24.2	3,300	*	6,640	7,930	11,730		

## Table 10: Summary of Discharges

\*Not calculated for this Flood Risk Project

			Peak Discharge (cfs)						
Flooding Source	Location	Drainage Area (Square Miles)	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance		
Corralitos Creek	Above confluence with Browns Creek	11.0	2,030	*	4,040	5,040	7,550		
Coward Creek	At confluence with Pajaro River	3.2	310	*	480	660	1,250		
Harkins Slough	At confluence with Pajaro River	9.8	860	*	1,920	2,540	4,140		
Harkins Slough	Above confluence with Gallighan Slough	6.3	650	*	1,380	1,800	2,760		
Moore Creek	At mouth	1.8	320	*	570	690	970		
Moore Creek	At State Highway 1	1.4	270	*	480	580	830		
Nobel Creek	At confluence with Soquel Creek	1.2	270	*	470	560	770		
Pajaro River	Downstream confluence with Salsipuedes Creek	1,275	14,250	*	32,500	43,600	76,200		
Rodeo Creek Gulch	At mouth	3.0	790	*	1,290	1,540	2,130		
Salsipuedes Creek	At confluence with Pajaro Creek	46.0	2,000 <sup>1</sup>	*	4,500 <sup>1</sup>	5,950 <sup>1</sup>	12,500 <sup>1</sup>		
San Lorenzo River	At mouth	136.0	23,700	*	42,300	50,600	70,100		

<sup>1</sup>Discharge loss downstream of Corralitos Creek occurs as independent overbank flow

			Peak Discharge (cfs)						
Flooding Source	Location	Drainage Area (Square Miles)	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance		
San Lorenzo River	Upstream of confluence with Branciforte Creek	118.0	22,000	*	39,600	47,600	66,500		
San Lorenzo River	At City of Santa Cruz corporate limits	116.0	21,700	*	39,300	47,200	66,100		
San Lorenzo River	Below confluence with Zayante Creek	106.0	18,800	*	35,000	42,600	60,700		
San Lorenzo River	Below confluence with Love Creek	60.8	12,300	*	23,800	29,200	42,700		
San Lorenzo River	Below confluence with Boulder Creek	51.2	9,390	*	18,800	23,400	34,800		
San Lorenzo River	Below confluence with Two Bar Creek	22.9	4,640	*	9,530	11,900	18,100		
San Vicente Creek	At mouth	11.3	1,240	*	2,340	2,850	4,140		
Schwans Lagoon	At East Cliff Lake Drive	1.1	765	*	1,106	1,290	1,715		
Soquel Creek	At mouth	42.8	8,310	*	14,700	17,500	24,300		
Soquel Creek	Upstream of confluence with Nobel Creek	41.6	8,240	*	14,600	17,400	24,200		

			Peak Discharge (cfs)					
Flooding Source	Location	Drainage Area (Square Miles)	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	
Struve Slough	At confluence with Watsonville Slough	2.8	240	*	540	700	1,120	
Struve Slough	Downstream of Harkins Slough Road	1.5	160	*	340	440	690	
Struve Slough	At Main Street	1.4	290 <sup>1</sup>	*	470 <sup>1</sup>	544 <sup>1</sup>	675 <sup>1</sup>	
Struve Slough	At Firethorn Way	0.9	231 <sup>1</sup>	*	374 <sup>1</sup>	433 <sup>1</sup>	536 <sup>1</sup>	
Struve Slough	Downstream of Landis Avenue	0.5	166 <sup>1</sup>	*	269 <sup>1</sup>	311 <sup>1</sup>	383 <sup>1</sup>	
Thomasello Creek	At confluence with Pajaro River	3.6	370	*	590	850	1,560	
Thompson Creek	At confluence with Pajaro River	5.3	520	*	700	1,000	1,870	
Watsonville Slough	At confluence with Pajaro River	19.4	1,280 <sup>1</sup>	*	2,940 <sup>1</sup>	3,890 <sup>1</sup>	6,580	
Watsonville Slough	Below confluence with Harkins Slough	15.6	1,320	*	2,980	3,910	6,400	
Watsonville Slough	Below confluence with Struve Slough	4.3	420	*	940	1,200	1,940	
Watsonville Slough	At Ford Street	1.3	227 <sup>2</sup>	*	368 <sup>2</sup>	426 <sup>2</sup>	529 <sup>2</sup>	

<sup>1</sup>Reduction in flow due to overbank storage

<sup>2</sup>Flows from hydrology study using Rational Method prepared by Philip Williams and Associates, Ltd. (PWA) in 2009

			Peak Discharge (cfs)					
Flooding Source	Location	Drainage Area (Square Miles)	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	
Watsonville Slough	At Main Street	1.0	220 <sup>1</sup>	*	356 <sup>1</sup>	412 <sup>1</sup>	511 <sup>1</sup>	
Watsonville Slough	NW corner of Watsonville Pioneer Cemetery	0.3	93 <sup>1</sup>	*	151 <sup>1</sup>	174 <sup>1</sup>	217 <sup>1</sup>	
Zayante Creek	At confluence with San Lorenzo River	26.2	6,250	*	10,100	11,800	15,600	
Zayante Creek	Below confluence with Bean Creek	26.1	6,150	*	9,990	11,700	15,500	
Zayante Creek	Below confluence with Lompico Creek	14.3	3,820	*	5,420	7,580	10,300	

<sup>1</sup>Flows from hydrology study using Rational Method prepared by Philip Williams and Associates, Ltd. (PWA) in 2009

## Figure 7: Frequency Discharge-Drainage Area Curves [Not Applicable to this Flood Risk Project]

## Table 11: Summary of Non-Coastal Stillwater Elevations

		Elevations (feet NAVD88)							
Flooding Source	Location	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance			
College Lake	Santa Cruz County, Unincorporated Areas	66.9	*	72.2	72.9	74.5			
Lake Tynan	Santa Cruz County, Unincorporated Areas	44.2	*	44.5	44.6	45.0			
Schwans Lagoon	Santa Cruz County, Unincorporated Areas	13.5	*	15.3	15.8	16.5			

\*Not calculated for this Flood Risk Project

		Agency		Drainage	Period of Record	
Flooding Source	Gage Identifier	that Maintains Gage	Site Name	Area (Square Miles)	From	То
Corralitos Creek	11159150	USGS	Near Corralitos	*	1958	1972
Corralitos Creek	11159200	USGS	Near Freedom	*	1955	1979
Green Valley Creek	11159400	USGS	Near Corralitos	*	1961	1973
Aptos Creek	11159700	USGS	At Aptos	*	1959	1972
West Branch Soquel Creek	11159800	USGS	Near Soquel	*	1959	1972
Soquel Creek	11160000	USGS	At Soquel	*	1937 1952	1937 1975
San Lorenzo River	11160020	USGS	Near Boulder Creek	*	1969	1978
Zayante Creek	11160300	USGS	At Zayante	*	1958	1978
San Lorenzo River	11160500	USGS	At Big Trees	*	1937	1978
Branciforte Creek	11161500	USGS	At Santa Cruz	*	1941 1953	1943 1968
Majors Creek	11161570	USGS	Near Santa Cruz	*	1970	1976
Laguna Creek	11161590	USGS	Near Davenport	*	1970	1976
San Vicente Creek	11161800	USGS	Near Davenport	*	1970	1978
Scott Creek	11159150	USGS	Above Little Creek near Davenport	*	1958	1972
Corralitos Creek	11159200	USGS	Near Corralitos at Freedom	*	1955	1976
Green Valley	11159400	USGS	Near Corralitos	*	1961	1973

Table 12: Stream Gage Information used to Determine Discharges

\*Data not available

#### 5.2 Hydraulic Analyses

Analyses of the hydraulic characteristics of flooding from the sources studied were carried out to provide estimates of the elevations of floods of the selected recurrence intervals. Base flood elevations on the FIRM represent the elevations shown on the Flood Profiles and in the Floodway Data tables in the FIS Report. Rounded whole-foot elevations may be shown on the FIRM in coastal areas, areas of ponding, and other areas with static base flood elevations. These whole-foot elevations may not exactly reflect the elevations derived from the hydraulic analyses. Flood elevations shown on the FIRM are primarily intended for flood insurance rating purposes. For construction and/or floodplain management purposes, users are cautioned to use the flood elevation data presented in this FIS Report in conjunction with the data shown on the FIRM. The hydraulic analyses for this FIS were based on unobstructed flow. The flood elevations shown on the profiles are thus considered valid only if hydraulic structures remain unobstructed, operate properly, and do not fail.

For streams for which hydraulic analyses were based on cross sections, locations of selected cross sections are shown on the Flood Profiles (Exhibit 1). For stream segments for which a floodway was computed (Section 6.3), selected cross sections are also listed on Table 24, "Floodway Data."

A summary of the methods used in hydraulic analyses performed for this project is provided in Table 13. Roughness coefficients are provided in Table 14. Roughness coefficients are values representing the frictional resistance water experiences when passing overland or through a channel. They are used in the calculations to determine water surface elevations. Greater detail (including assumptions, analysis, and results) is available in the archived project documentation.

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Aptos Creek	Approximately 60 feet upstream of the confluence with the Pacific Ocean	Approximately 0.8 mile upstream of Soquel Drive	USGS Regional Regression Equation and Log-Pearson Type III	USACE HEC-2	1983	A, AE w/ Floodway	For Log-Pearson III analysis USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). Starting WSELs is mean higher high water elevation.
Arana Gulch	Approximately 3,000 feet downstream of Capitola Road	Approximately 100 feet upstream of Brookwood Drive	USGS Regional Regression Equation and Log-Pearson Type III	USACE HEC-2	1983	AE w/ Floodway	For Log-Pearson III analysis USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). For urbanized watershed, results were adjusted to account for the effects of urbanization on peak flood flow. The adjustment for urbanization is a function of the percentage of basin developed and the percentage of channels for which storm sewers were constructed (DOI 1977). Adjustments for urbanization were required on Arana Gulch within Santa Cruz. Starting WSELs were based on manual computations which considered culvert and weir flow at the northern end of the small craft harbor.
Baldwin Creek	Confluence with Pacific Ocean	At Coast Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	

# Table 13: Summary of Hydrologic and Hydraulic Analyses

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Bean Creek	Confluence with Zayante Creek	Approximately 87 feet upstream of Bean Creek Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Boulder Creek	Confluence with San Lorenzo River	Approximately 2,720 feet upstream of Big Basin Highway	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Branciforte Creek	Confluence with San Lorenzo River	Approximately 1,088 feet upstream of Ocean Street	USGS Regional Regression Analysis and Log-Pearson Type III	Slope-Area Method	1983	A, AE	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were determined by regional regression analysis for basins with little or no impoundment storage or regulation. The method used for regression analysis was developed by the USGS (DOI 1977). The regression relationships predict peak flood flow for each average recurrence interval as a function of basin area, normal annual basin precipitation, and average basin elevation. Other basin characteristics were found to be statistically insignificant for prediction of peak flood flows. WSELs were calculated using the slope-area method.
Browns Creek	Confluence with Corralitos Creek	Approximately 1,950 feet upstream of Via del Sol	USACE HEC-1	USACE HEC-2	1983	A	For the Pajaro Valley streams, peak flood flows for the 10-, 2-, 1-, and 0.2-percent- annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Carbonera Creek	Confluence with Branciforte Creek	Approximately 50 feet upstream of Carbonera Drive	Log-Pearson Type III	HEC-2	1982	AE w∕ Floodway	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). Starting WSELs were calculated using the slope-area method.
Carbonera Creek	Approximately 50 feet upstream of Carbonera Drive	Approximately 1.5 miles upstream of State Highway 17	USGS Regional Regression Analysis and Log-Pearson Type III	Slope-Area Method	1982	A, AE w∕ Floodway	For urbanized watershed, results were adjusted to account for the effects of urbanization on peak flood flow. The adjustment for urbanization is a function of the percentage of basin developed and the percentage of channels for which storm sewers were constructed (DOI 1977). Adjustments for urbanization were required on Carbonera Creek within City of Santa Cruz.
College Lake	Confluence with Corralitos Creek	Approximately 2,600 feet upstream of Paulsen Road	USACE HEC-1	USACE HEC-2	1983	AE	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Corralitos Creek	Lake Avenue	Approximately 355 feet upstream of confluence with Mormon Gulch	USACE HEC-1	USACE HEC-2	1983	A, AE w/ Floodway	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Coward Creek	Confluence with the Pajaro River	Approximately 4,450 feet upstream of Riverside Road	USACE HEC-1	USACE HEC-2	1983	AE	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Drew Lake	At College Road	Approximately 3,320 feet upstream of College Road	USACE HEC-1	USACE HEC-2	1983	A	For the Pajaro Valley streams, peak flood flows for the 10-, 2-, 1-, and 0.2-percent- annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Gallighan Slough	Confluence with Harkins Slough	Approximately 0.5 mile upstream of confluence with Harkins Slough	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Hanson Slough	Confluence with Watsonville Slough	Approximately 1 mile upstream of confluence with Watsonville Slough	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Hare Creek	Confluence with Boulder Creek	Approximately 0.6 mile upstream of confluence with Boulder Creek	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Harkins Slough	Confluence with Watsonville Slough	Approximately 0.7 mile upstream of Dunlap Lane	USACE HEC-1	USACE HEC-2	1983	A, AE w/ Floodway	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Hopkins Gulch	Confluence with Bear Creek	Approximately 23 feet upstream of Wicket Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Kelly Lake	At College Road	Approximately 4,020 feet upstream of College Road	USACE HEC-1	USACE HEC-2	1983	A	For the Pajaro Valley streams, peak flood flows for the 10-, 2-, 1-, and 0.2-percent- annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Kings Creek	Confluence with San Lorenzo River	Approximately 0.7 mile upstream of Highway 9	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Laguna Creek	Confluence with Pacific Ocean	Approximately 3,040 feet upstream of confluence with Pacific Ocean	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Lake Tynan	Approximately 4,500 feet upstream of Riverside Road	Approximately 900 feet downstream of Lakeview Road	USACE HEC-1	USACE HEC-2	1983	AE	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Loch Lomond Reservoir	Approximately 200 feet upstream of Newell Creek Road	Approximately 2.4 miles upstream of Newell Creek Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Lompico Creek	At mouth	Approximately 2.7 miles upstream from mouth	Central Coast Region USGS Regression Equations	HEC-RAS 3.1.2	2011	A	An approximate study was conducted on Lompico Creek for a total of 2.7 miles from the mouth of the stream to the point at which the basin drains 1 square mile. Discharges for the 1-percent-annual-chance recurrence interval for the approximate study done on Lompico Creek was determined using the Central Coast Region USGS regression equations for California as described in the USGS Water-Resources Investigations Report 77-21 (DOI 1977). Analysis of the hydraulic characteristics of flooding for the approximate study was carried out to profile estimates of the elevations of floods of the selected recurrence intervals.

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Lompico Creek (continued)	At mouth	Approximately 2.7 miles upstream from mouth	Central Coast Region USGS Regression Equations	HEC-RAS 3.1.2	2011	A	Water-surface profiles were computed for enhanced approximate and approximate study streams through the use of the U.S. Army Corps of Engineers HEC-RAS version 3.1.2 computer program (USACE 2004). Water surface profiles were produced for the 1- percent-annual-chance storms for Lompico Creek. The enhanced approximate and approximate study methodology used Watershed Information System (WISE) as a preprocessor to HEC-RAS. Tools within WISE allowed the engineer to verify that the cross-section data was acceptable (AECOM 2008). The WISE program was used to generate the input data file for cross section of the modeled stream. No floodway was calculated for Lompico Creek since it was studied by approximate methods.
Love Creek	Approximately 900 feet upstream of Brookside Avenue	Approximately 1,560 feet upstream of Love Creek Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Majors Creek	Confluence with Pacific Ocean	Approximately 780 feet upstream of State Highway 1	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Mill Creek	Confluence with Scott Creek	Approximately 880 feet upstream of Swanton Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Molino Creek	Confluence with Pacific Ocean	Approximately 0.6 mile upstream of Swanton Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Moore Creek	Approximately 2,304 feet downstream of Delaware Avenue	Approximately 920 feet upstream of State Highway 1	USGS Regional Regression Analysis	USACE HEC-2	1983	A, AE w/ Floodway	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were determined by regional regression analysis for basins with little or no impoundment storage or regulation. The method used for regression analysis was developed by the USGS (DOI 1977). The regression relationships predict peak flood flow for each average recurrence interval as a function of basin area, normal annual basin precipitation, and average basin elevation. Other basin characteristics were found to be statistically insignificant for prediction of peak flood flows. A starting elevation equal to mean higher high water at Monterey Bay in the Pacific Ocean was used.
Moran Lake	At East Cliff Drive	Approximately 1,447 feet upstream of East Cliff Drive	USGS Regional Regression Equation Analysis and Log-Pearson Type III	*	1983	А	
Newell Creek	Confluence with San Lorenzo River	At Loch Lomond Reservoir	USGS Regional Regression Equation Analysis and Log-Pearson Type III	*	1983	A	

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Nobel Creek	Approximately 2,920 feet downstream of Private Drive	Approximately 740 feet upstream of Private Bridge	USGS Regional Regression Analysis	Step- backwater	1983	AE w/ Floodway	Peak flood flows for the 10-, 2-, 1-, and 0.2- percent-annual-chance storm events were determined by regional regression analysis for basins with little or no impoundment storage or regulation. The method used for regression analysis was developed by the USGS (DOI 1977). The regression relationships predict peak flood flow for each average recurrence interval as a function of basin area, normal annual basin precipitation, and average basin elevation. Other basin characteristics were found to be statistically insignificant for prediction of peak flood flows. The WSELs from the mouth of Nobel Creek to the upstream end of the 1,700-foot culvert were computed by manual calculations using the standard step-backwater method. The starting WSEL for Nobel Creek was assumed to be the 10-percent-annual-chance elevation at the confluence with Soquel Creek.
Old Dairy Gulch	Confluence with Pacific Ocean	Approximately 1,775 feet upstream of Union Pacific Railroad	USGS Regional Regression Equation Analysis and Log-Pearson Type III	*	1983	A	
Pajaro River	Approximately 800 feet downstream of the confluence with Watsonville Slough	Approximately 0.8 mile upstream of Riverside Drive	USACE HEC-1	USACE HEC-2	1983	A, AE w/ Floodway	For the City of Watsonville, peak flood flows in the Pajaro River basin for the 10-, 2-, 1-, and 0.2-percent-annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Physical characteristics and the relationships developed during calibration were used to derive Clark unit hydrograph parameters for all subbasins defined for this study.

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Pajaro River (continued)	Approximately 800 feet downstream of the confluence with Watsonville Slough	Approximately 0.8 mile upstream of Riverside Drive	USACE HEC-1	USACE HEC-2	1983	A, AE w/ Floodway	Hypothetical 1- and 0.2-percent-annual- chance rainfall hyetographs were developed using published intensity-duration-frequency curves (State of California DWR 1975). Starting WSELs is mean higher high water elevation. Because the Pajaro River levees do not provide 3 feet of freeboard with respect to the 1-percent-annual-chance flood, WSELs were computed for two cases. In the first case, flood elevations were computed before levee overtopping begins, assuming the levees remained intact. In the second case, floods were computed after overtopping occurs, assuming the levees had failed. According to FEMA guidelines, the worst case is used to establish flood elevations in the channel and in the floodplain area. In this study, WSELs along the Pajaro River before levee overtopping were always highest for the channel, while the highest elevations for the floodplain area were computed when the levees were assumed to be overtopped. The location of levee failure cannot be predicted under major floods; therefor, it was assumed that all levees fail.
Pinto Lake	Approximately 1,088 feet upstream of Green Valley Road	Approximately 1 mile upstream of Green Valley Road	USACE HEC-1	USACE HEC-2	1983	A	For the Pajaro Valley streams, peak flood flows for the 10-, 2-, 1-, and 0.2-percent- annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Rodeo Creek Gulch	East Cliff Drive	Approximately 1,600 feet upstream of Soquel Drive	Log-Pearson Type III	USACE HEC-2	1983	AE w/ Floodway	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). Starting WSELs is mean higher high water elevation.
Rose Reservoir	Approximately 730 feet upstream of Casserly Road	Approximately 1,390 feet upstream of Casserly Road	USACE HEC-1	USACE HEC-2	1983	A	For the Pajaro Valley streams, peak flood flows for the 10-, 2-, 1-, and 0.2-percent- annual-chance storm events were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Salsipuedes Creek	Confluence with the Pajaro River	College Lake Outlet	Rational and Regional Regression Methods	HEC-RAS 4.0 (USACE 2008)	2009	AE	Peak discharges for Salsipuedes Creek were utilized from the published FIS and no new hydrology analysis was conducted. The downstream boundary water surface elevations were determined from the effective HEC-2 study. No upstream boundary conditions were included in the hydraulic modeling because all events were modeled using a subcritical flow regime. Because the Salsipuedes Creek levees do not provide 3 feet of freeboard with respect to the 1-percent-annual-chance flood, WSELs were computed for two cases. In the first case, flood elevations were computed before levee overtopping begins, assuming the levees remained intact. In the second case, floods were computed after overtopping occurs, assuming the levees had failed.

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Salsipuedes Creek (continued)	Confluence with the Pajaro River	College Lake Outlet	Rational and Regional Regression Methods	HEC-RAS 4.0 (USACE 2008)	2009	AE	According to FEMA guidelines, the worst case is used to establish flood elevations in the channel and in the floodplain area. In this study, WSELs along the Salsipuedes Creek before levee overtopping were always highest for the channel, while the highest elevations for the floodplain area were computed when the levees were assumed to be overtopped. The location of levee failure cannot be predicted under major floods; therefor, it was assumed that all levees fail.
San Lorenzo River	Confluence with the Pacific Ocean	Approximately 215 feet upstream of Highway 9	USGS Regional Regression Equation Analysis and Log-Pearson Type III	USACE HEC-2	1983	A, AE w/ Floodway	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). A starting elevation equal to mean higher high water at Monterey Bay in the Pacific Ocean was used. Because the San Lorenzo River levees do not provide 3 feet of freeboard with respect to the 1-percent-annual-chance flood, WSELs were computed for two cases. In the first case, flood elevations were computed before levee overtopping begins, assuming the levees remained intact. In the second case, floods were computed after overtopping occurs, assuming the levees had failed. According to FEMA guidelines, the worst case is used to establish flood elevations in the channel and in the floodplain area. In this study, computed WSELs along the San Lorenzo River before levee overtopping were the highest for the channel except for a section between Riverside Drive and the mouth.

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
San Lorenzo River (continued)	Confluence with the Pacific Ocean	Approximately 215 feet upstream of Highway 9	USGS Regional Regression Equation Analysis and Log-Pearson Type III	USACE HEC-2	1983	A, AE w/ Floodway	Highest WSELs for this section of the channel and all floodplain areas were computed when the levees were assumed to be overtopped. USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977).
San Vicente Creek	Confluence with the Pacific Ocean	Approximately 3,700 feet upstream of State Highway 1	USGS Regional Regression Equation and Log-Pearson Type III	USACE HEC-2	1983	A, AE w/ Floodway	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). The starting WSEL for San Vicente Creek was determined by critical-depth computations.
Schwans Lagoon	Approximately 350 feet downstream of East Cliff Drive	Approximately 1,700 feet upstream of East Cliff Drive	Log-Pearson Type III	USACE HEC-2	1983	AE	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). Starting WSELs for Schwans Lagoon were based on manual computations which considered culvert and weir flow at East Cliff Drive.
Scott Creek	At Coast Road	Approximately 2,835 feet upstream of Purdy Ranch Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Soquel Creek	Approximately 500 feet downstream of Stockton Avenue	Approximately 1,700 feet upstream of Soquel Creek Road	USGS Regional Regression Equation and Log-Pearson Type III	USACE HEC-2	1983	A, AE w/ Floodway	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). The flows on Soquel Creek resulting from the regression equations were adjusted to correspond with the flows predicted form the data at two gages. The starting WSEL for Soquel Creek was assumed to equal the mean higher high water elevation at Monterey Bay in the Pacific Ocean.
Struve Slough	Confluence with Watsonville Slough	Near the concrete culvert outlet at South Green Valley Road	Rational Method	HEC-RAS 4.0 (USACE 2008)	2009	AE w/ Floodway	New hydrologic analysis was carried out to establish peak discharge-frequency relationships. Peak flood discharges for the 10-, 2-, 1-, and 0.2- percent annual-chance storm events were calculated using the Rational Method and also using Regional Regression equations, then both sets of values were compared to the peak discharges obtained from the published FIS or from the effective hydraulic models. The peak discharges determined by the Rational Method were found to be the most appropriate for the study locations and closest to the published flows. The hydraulic model boundary conditions were established without regard for the regulatory Pajaro River floodplain. Given the variation in watershed size between the Pajaro River and the study flood sources, it was determined that peak flooding would not be coincident.

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Struve Slough (continued)	Confluence with Watsonville Slough	Near the concrete culvert outlet at South Green Valley Road	Rational Method	HEC-RAS 4.0 (USACE 2008)	2009	AE w/ Floodway	Water surface elevations for the downstream end were determined from location hydraulics studies conducted for Harkins Slough Road bridge crossings.
Thomasello Creek	Approximately 1,000 feet upstream of the confluence with the Pajaro River	Approximately 1,000 feet upstream of State Highway 129	USACE HEC-1	USACE HEC-2	1983	AE	Peak flows were based on rainfall-runoff computations using the USACE HEC-1 computer model (USACE 1968). Calibration of rainfall-runoff parameters employed in the HEC-1 computer model was performed using the techniques described in the HEC-1 user documentation (USACE January 1973).
Thompson Creek	Confluence with the Pajaro River	Approximately 3,800 feet upstream of Carlton Road	Log-Pearson Type III	USACE HEC-2	1983	AE	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). On gaged stream, peak flows generated from the regional regression analysis were adjusted to match the USGS log-Pearson Type III estimates at the gage. On ungagged streams, the peak flows generated from the regional regression analysis were used without adjustment.
Two Bar Creek	Confluence with San Lorenzo River	Approximately 0.6 mile upstream of Highway 9	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Waddell Creek	Confluence with Pacific Ocean	Approximately 2,8 miles upstream of Coast Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
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Watsonville Slough	Confluence with the Pajaro River	Northwest corner of Watsonville Pioneer Cemetery	Rational Method	HEC-RAS 4.0 (USACE 2008)	2009	AE w/ Floodway	New hydrologic analysis was carried out to establish peak discharge-frequency relationships for Watsonville Slough. Peak flood discharges for the 10-, 2-, 1-, and 0.2- percent annual-chance storm events were calculated using the Rational Method and also using Regional Regression equations, then both sets of values were compared to the peak discharges obtained from the published FIS or from the effective hydraulic models. The peak discharges determined by the Rational Method were found to be the most appropriate for the study locations and closest to the published flows. The hydraulic model boundary conditions were established without regard for the regulatory Pajaro River floodplain. Given the variation in watershed size between the Pajaro River and the study flood sources, it was determined that peak flooding would not be coincident. Water surface elevations for the downstream end were determined from location hydraulics studies conducted for Harkins Slough Road bridge crossings. WSELs, south of Ford Road, are influenced by those on the Pajaro River.
West Branch Struve Slough	Confluence with Struve Slough	Approximately 1,460 feet upstream of Harkins Slough Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	
Wilder Creek	Confluence with Pacific Ocean	Approximately 1,720 feet upstream of Coast Road	USGS Regional Regression Equation and Log-Pearson Type III	*	1983	A	

Flooding Source	Study Limits Downstream Limit	Study Limits Upstream Limit	Hydrologic Model or Method Used	Hydraulic Model or Method Used	Date Analyses Completed	Flood Zone on FIRM	Special Considerations
Zayante Creek	Confluence with the San Lorenzo River	Approximately 2,066 feet upstream of East Zayante Road	Regional Regression Equation and Log-Pearson Type III	USACE HEC-2	1983	A, AE w/ Floodway	USGS regional skew estimates were used, rather than the U.S. Water Resources Council (USWRC) regional skew estimates, because the former values gave results that were more consistent for streams in the study area (USWRC 1977). On gaged stream, peak flows generated from the regional regression analysis were adjusted to match the USGS log-Pearson Type III estimates at the gage. On ungagged streams, the peak flows generated from the regional regression analysis were used without adjustment.

\*Data not available

Flooding Source	Channel "n"	Overbank "n"
Arana Gulch	0.040 - 0.050	0.060 – 0.100
Branciforte Creek	0.040 - 0.050	0.060 – 0.100
Carbonera Creek	0.050	0.10
Corralitos Creek	0.040 - 0.050	0.045 – 0.100
Moore Creek	0.040 - 0.050	0.060 – 0.100
Nobel Creek	0.035	0.100
Pajaro River	0.015 – 0.050	0.045 – 0.100
Salsipuedes Creek	0.040 – 0.050	0.045 – 0.100
San Lorenzo River	0.020 - 0.040	0.100
Soquel Creek	0.040	0.100
Struve Slough	0.025 - 0.068	0.022 - 0.068
Watsonville Slough	0.015 – 0.045	0.045 – 0.100

**Table 14: Roughness Coefficients** 

#### 5.3 Coastal Analyses

For the areas of Santa Cruz County that are impacted by coastal flooding processes, coastal flood hazard analyses were performed to provide estimates of coastal BFEs. Coastal BFEs reflect the increase in water levels during a flood event due to extreme tides and storm surge as well as overland wave effects.

The following subsections provide summaries of how each coastal process was considered for this FIS Report. Greater detail (including assumptions, analysis, and results) is available in the archived project documentation. Table 15 summarizes the methods and/or models used for the coastal analyses. Refer to Section 2.5.1 for descriptions of the terms used in this section.

Flooding Source	Study Limits From	Study Limits To	Hazard Evaluated	Model or Method Used	Date Analysis was Completed
Pacific Ocean	South San Mateo County Border	North Monterey County Border	Wave Runup	FEMA Pacific Guidelines (2005), Stockdon, DIM, and TAW	8/9/2013

**Table 15: Summary of Coastal Analyses** 

#### 5.3.1 Total Stillwater Elevations

The total stillwater elevations (stillwater including storm surge plus wave setup) for the 1% annual chance flood were determined for areas subject to coastal flooding. The models and methods that were used to determine storm surge and wave setup are listed in Table 15. The

stillwater elevation that was used for each transect in coastal analyses is shown in Table 17, "Coastal Transect Parameters." Figure 8 shows the total stillwater elevations for the 1% annual chance flood that was determined for this coastal analysis.



Figure 8: 1% Annual Chance Total Stillwater Elevations for Coastal Areas

#### Astronomical Tide

Astronomical tidal statistics were generated directly from local tidal constituents by sampling the predicted tide at random times throughout the tidal epoch.

#### Storm Surge Statistics

Storm surge is modeled based on characteristics of actual storms responsible for significant coastal flooding. The characteristics of these storms are typically determined by statistical study of the regional historical record of storms or by statistical study of tidal gages.

When historic records are used to calculate storm surge, characteristics such as the strength, size, track, etc., of storms are identified by site.

Tidal gages can be used instead of historic records of storms when the available tidal gage record for the area represents both the astronomical tide component and the storm surge component. Table 16 provides the gage name, managing agency, gage type, gage identifier, start date, end date, and statistical methodology applied to each gage used to determine the stillwater elevations.

Gage Name	Managing Agency of Tide Gage Record	Gage Type	Start Date	End Date	Statistical Methodology
San Francisco (9414290)	NOAA	Tide	1854	Present	GEV
Monterey (9413450)	NOAA	Tide	1973	Present	GEV

Table 16: Tide Gage Analysis Specifics

#### Wave Setup Analysis

Wave setup was computed during the storm surge modeling through the methods and models listed in Table 15 and included in the frequency analysis for the determination of the total stillwater elevations.

#### 5.3.2 Waves

An integral component of the transect-based TWL analysis is an accurate determination of the offshore and nearshore wave climate. A continuous 50-year hourly deep-water wave hindcast was developed by Oceanweather Inc. using reanalysis of historical wind fields. Three nested model grid components of sequentially higher resolution were used to resolve wave conditions of varying spatial scales, including basin (global), regional (Northeast Pacific Ocean), and coastal (California) grids.

The deep-water dataset was further transformed to reflect nearshore conditions at the edge of the surf zone in approximately 33-49 feet water depth. The nearshore wave transformation component was carried out by the Scripps Institute of Oceanography (SIO) Coastal Data Information Program (CDIP) research group in collaboration with BakerAECOM using the SIO SHELF model. The output from this wave transformation model provides the input conditions for the 1-D transect-based coastal hazard analysis used to calculate BFEs.

#### 5.3.3 Coastal Erosion

A single storm episode can cause extensive erosion in coastal areas. Storm-induced erosion was evaluated to determine the modification to existing topography that is expected to be associated with flooding events. Erosion was evaluated using the methods listed in Table 15.

#### 5.3.4 Wave Hazard Analyses

Overland wave hazards were evaluated to determine the combined effects of ground elevation, vegetation, and physical features on overland wave propagation and wave runup. These analyses were performed at representative transects along all shorelines for which waves were expected to be present during the floods of the selected recurrence intervals. The results of these analyses were used to determine elevations for the 1% annual chance flood.

Transect locations were chosen with consideration given to the physical land characteristics as well as development type and density so that they would closely represent conditions in their locality. Additional consideration was given to changes in the total stillwater elevation. Transects were spaced close together in areas of complex topography and dense development or where total stillwater elevations varied. In areas having more uniform characteristics, transects were spaced at larger intervals. Transects shown in Figure 9, "Transect Location Map," are also depicted on the FIRM. Table 17 provides the location, stillwater elevations, and starting wave conditions for each transect evaluated for overland wave hazards. In this table, "starting" indicates the parameter value at the beginning of the transect.

#### Wave Height Analysis

Wave height analyses were performed to determine wave heights and corresponding wave crest elevations for the areas inundated by coastal flooding and subject to overland wave propagation hazards. Refer to Figure 6 for a schematic of a coastal transect evaluated for overland wave propagation hazards.

Wave heights and wave crest elevations were modeled using the methods and models listed in Table 15, "Summary of Coastal Analyses".

#### Wave Runup Analysis

Wave runup analyses were performed to determine the height and extent of runup beyond the limit of stillwater inundation for the 1% annual chance flood. Wave runup elevations were modeled using the methods and models listed in Table 15.

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water Elevation (feet NAVD88) <sup>1</sup>					
Transect	x	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
1	562936.73	4106694.48	17.5	18.7	19.5	20.4	22.5	VE	20
2	563586.36	4105987.25	27.9	31.9	34.9	37.9	45.0	VE	38
3	563826.60	4105660.35	18.7	20	21.0	22.0	24.4	VE	22
4	564022.10	4105394.81	17.9	19	19.8	20.6	22.4	VE	21
5	564204.34	4104894.05	14.7	15.7	16.4	17.1	18.9	VE	17
6	565252.66	4103498.33	15.4	16.4	17.2	18.0	19.7	VE	18
7	566962.16	4101097.64	14.8	16.4	17.9	19.7	25.2	VE	20

#### Table 17: Coastal Transect Parameters

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Wate	r Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	Х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
8	568374.41	4099482.18	20.6	21.6	22.4	23.1	24.8	VE	23
9	569548.78	4097659.85	18.5	19.5	20.3	21.2	23.2	VE	21
10	571136.08	4096365.59	14.9	15.7	16.3	16.8	17.9	VE	17
11	573130.75	4094677.48	16.5	17.4	18.0	18.6	20.0	VE	19
12	574942.89	4093240.53	16.6	17.7	18.6	19.5	21.7	VE	19*
13	576345.12	4092435.27	18.3	19.4	20.1	20.9	22.7	VE	21
14	576544.20	4092230.22	20.7	22.7	24.4	26.3	31.7	VE	26
15	578249.49	4091095.24	16.4	17.3	18.1	18.9	20.6	VE	19

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
16	580194.09	4090186.00	18.5	21.6	24.2	27.1	35.2	VE	27
17	582017.76	4089940.50	14.3	15.3	16.2	17.1	19.7	VE	17
18	583253.50	4089443.20	25.7	28.1	29.9	31.6	35.5	VE	32
19	583604.68	4089552.88	18.4	20.3	22.0	24.0	29.9	VE	24
20	583753.29	4089592.24	26.6	28.9	30.5	32.1	35.5	VE	32
21	584187.36	4089571.50	32.0	34.3	36.0	37.6	41.3	VE	38
22	584556.42	4089558.15	23.1	26.0	28.2	30.5	36.2	VE	31
23	585274.17	4089821.31	17.6	20.7	23.7	27.3	38.8	VE	27

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
24	585745.78	4089959.83	28.9	30.8	32.2	33.6	36.7	VE	34
25	586279.01	4089793.87	28.8	30.5	31.6	32.6	34.4	VE	33
26	586870.63	4090093.24	20.2	21.8	23.0	24.3	27.2	VE	24
27	586910.31	4090285.03	24.0	26.0	27.6	29.3	33.3	VE	29
28	586897.42	4090545.40	25.7	28	29.9	32.0	37.8	VE	32
29	586886.12	4090787.46	11.1	11.7	12.2	12.9	14.5	VE	13
30	587218.06	4091071.50	15.3	16.1	16.8	17.6	19.5	VE	18
31	587631.98	4091125.40	15.0	16.2	17.2	18.4	21.8	VE	18

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
32	588567.66	4091047.06	16.7	17.6	18.4	19.1	21.0	VE	19
33	589197.35	4090964.21	16.2	17.2	18.0	18.8	21.0	VE	19
34	589411.81	4090857.97	17.2	18.3	19.3	20.4	23.1	VE	20
35	589548.14	4090775.33	14.5	15.5	16.3	17.1	19.4	VE	17
36	589697.61	4090720.08	24.6	26.8	28.7	30.8	36.4	VE	31
37	590256.59	4090733.74	15.7	16.8	17.8	18.8	21.6	VE	19
38	590410.56	4090641.77	15.8	16.6	17.3	18.0	19.7	VE	18
39	590679.46	4090498.35	17.7	18.6	19.4	20.1	21.9	VE	20

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Wate	r Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	Х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
40	590857.98	4090378.16	17.2	18.1	18.8	19.5	21.1	VE	20
41	590981.63	4090274.63	25.5	27.9	29.7	31.4	35.5	VE	31
42	591426.12	4090200.99	35.7	38.3	40.0	41.7	45.2	VE	42
43	591826.55	4090457.09	18.3	20.2	21.6	23.0	26.5	VE	23
44	591959.32	4090562.18	28.8	31.0	32.7	34.5	39.0	VE	35
45	592639.73	4091255.58	24.9	26.7	28.0	29.4	32.8	VE	29
46	592953.67	4091676.44	13.2	14.1	14.9	15.7	17.9	VE	16
47	593197.20	4091993.83	16.0	17.0	17.7	18.5	20.2	VE	18*

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
48	593415.36	4092091.33	16.5	17.7	18.6	19.6	22.0	VE	20
49	593577.47	4092157.36	17.7	19.9	21.8	24.1	30.5	VE	24
50	593953.81	4092427.56	18.2	19.7	20.9	22.3	25.6	VE	22
51	594561.05	4092826.06	16.9	18.0	18.9	19.7	21.7	VE	20
52	595109.81	4092850.91	20.0	21.3	22.3	23.2	25.3	VE	23
53	595289.68	4092802.42	16.6	17.7	18.5	19.2	21.0	VE	19
54	595655.96	4092678.76	21.6	23.0	24.0	25.1	27.4	VE	25
55	596354.80	4092332.23	19.4	20.8	22.0	23.2	26.0	VE	23

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>						
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)			
56	597307.01	4091831.29	21.1	22.9	24.3	25.7	29.1	VE	26			
57	597560.42	4091676.22	18.1	19.4	20.4	21.4	23.7	VE	21			
58	597861.90	4091430.35	17.9	19.1	20.0	21.0	23.1	VE	21			
59	598300.38	4091050.13	18.4	19.7	20.8	21.9	24.6	VE	22			
60	599003.53	4090354.47	16.7	17.8	18.7	19.6	21.7	VE	20			
61	599290.49	4090051.14	18.2	19.4	20.3	21.2	23.2	VE	21			
62	600293.13	4088874.83	20.2	21.3	22.0	22.7	24.2	VE	23			
63	600854.39	4088094.31	16.3	17.1	17.6	18.1	19.2	VE	18			

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>						
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)			
64	601418.44	4087289.01	18.5	19.5	20.3	21.1	23.1	VE	21			
65	601790.27	4086590.05	14.1	14.8	15.3	15.8	16.8	VE	16			
66	601987.16	4086233.17	16.9	17.9	18.8	19.6	21.7	VE	20			
67	602726.73	4084816.27	17.8	18.7	19.3	19.9	21.1	VE	20			
68	603504.06	4083420.77	17.1	17.8	18.3	18.8	19.7	VE	19			
69	604261.08	4082016.35	16.0	16.8	17.5	18.2	19.7	VE	18			
70	604779.25	4080941.63	16.5	17.4	18.2	19.0	20.8	VE	19			
71	605303.08	4079865.63	19.0	20.3	21.3	22.1	23.8	VE	22			

	X,Y Co (Meters, NAD8	ordinates 3 UTM Zone 10)		Total Water	Elevation (fee	t NAVD88) <sup>1</sup>			
Transect	х	Y	10% Annual Chance	4% Annual Chance	2% Annual Chance	1% Annual Chance	0.2% Annual Chance	Zone	BFE (ft)
72	605694.94	4079029.13	18.4	19.7	20.5	21.2	22.6	VE	21

<sup>1</sup>North American Vertical Datum of 1988

\*Value has been rounded to the nearest tenth of a foot – precision of results to the hundredths of a foot resulted in rounding the BFE on the FIRM down to the nearest whole foot.







Map Projection:

Universal Transeverse Mercator Zone 10 North; North American Datum 1983





Transect Location Map

#### PANELS WITH TRANSECTS:

0156F, 0157F, 0159F, 0186F, 0189F, 0306F, 0307F, 0328F, 0329F, 0333F, 0334F, 0352F, 0353F, 0354F, 0356F, 0357F, 0358F, 0359F, 0378F, 0386F, 0388F, 0389F, 0452F, 0456F



Figure 9: Transect Location Map, continued



	1	inch = 6	6,055 fee	et		1:72,661
Ñ	0	1,750	3,500	7,000	10,500	Feet 14,000

Map Projection:

Universal Transeverse Mercator Zone 10 North; North American Datum 1983



## NATIONAL FLOOD INSURANCE PROGRAM

Transect Location Map

#### PANELS WITH TRANSECTS:

0156F, 0157F, 0159F, 0186F, 0189F, 0306F, 0307F, 0328F, 0329F, 0333F, 0334F, 0352F, 0353F, 0354F, 0356F, 0357F, 0358F, 0359F, 0378F, 0386F, 0388F, 0389F, 0452F, 0456F



#### 5.4 Alluvial Fan Analyses

This is section is not applicable to this Flood Risk Project.

Table 18: Summary of Alluvial Fan Analyses[Not Applicable to this Flood Risk Project]

Table 19: Results of Alluvial Fan Analyses[Not Applicable to this Flood Risk Project

# FEDERAL EMERGENCY MANAGEMENT AGENCY

## **VOLUME 2 OF 3**



# SANTA CRUZ COUNTY, CALIFORNIA AND INCORPORATED AREAS

COMMUNITY NAME	COMMUNITY NUMBER	
CAPITOLA, CITY OF	060354	
SANTA CRUZ, CITY OF	060355	
SANTA CRUZ COUNTY UNINCORPORATED AREAS	060353	
SCOTTS VALLEY, CITY OF	060356	
WATSONVILLE, CITY OF	060357	



# REVISED: SEPTEMBER 29, 2017

FLOOD INSURANCE STUDY NUMBER 06087CV002C

Version Number 2.3.2.0

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Moore Creek	24-26 P
Nobel Creek	27-28 P

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Thomasello Creek	74 P
Thompson Creek	75 P
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#### **Published Separately**

Flood Insurance Rate Map (FIRM)

#### **SECTION 6.0 – MAPPING METHODS**

#### 6.1 Vertical and Horizontal Control

All FIS Reports and FIRMs are referenced to a specific vertical datum. The vertical datum provides a starting point against which flood, ground, and structure elevations can be referenced and compared. Until recently, the standard vertical datum used for newly created or revised FIS Reports and FIRMs was the National Geodetic Vertical Datum of 1929 (NGVD29). With the completion of the North American Vertical Datum of 1988 (NAVD88), many FIS Reports and FIRMs are now prepared using NAVD88 as the referenced vertical datum.

Flood elevations shown in this FIS Report and on the FIRMs are referenced to NAVD88. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between NGVD29 and NAVD88 or other datum conversion, visit the National Geodetic Survey website at www.ngs.noaa.gov, or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 (301) 713-3242

Temporary vertical monuments are often established during the preparation of a flood hazard analysis for the purpose of establishing local vertical control. Although these monuments are not shown on the FIRM, they may be found in the archived project documentation associated with the FIS Report and the FIRMs for this community. Interested individuals may contact FEMA to access these data.

To obtain current elevation, description, and/or location information for benchmarks in the area, please contact information services Branch of the NGS at (301) 713-3242, or visit their website at www.ngs.noaa.gov.

A countywide conversion factor of +2.75 feet was calculated for Santa Cruz County.

# Table 20: Countywide Vertical Datum Conversion

[Not Applicable to this Flood Risk Project]

# Table 21: Stream-Based Vertical Datum Conversion[Not Applicable to this Flood Risk Project]

#### 6.2 Base Map

The FIRMs and FIS Report for this project have been produced in a digital format. The flood hazard information was converted to a Geographic Information System (GIS) format that meets FEMA's FIRM database specifications and geographic information standards. This information is provided in a digital format so that it can be incorporated into a local GIS and be accessed more easily by the community. The FIRM Database includes most of the tabular information contained in the FIS Report in such a way that the data can be associated with pertinent spatial features. For example, the information contained in the Floodway Data table and Flood Profiles can be linked to the cross sections that are shown on the FIRMs. Additional information about the FIRM Database and its contents can be found in FEMA's *Guidelines and Standards for Mapping Partners*, www.fema.gov/guidelines-and-standards-flood-risk-analysis-and-mapping.

Base map information shown on the FIRM was derived from the sources described in Table 22.

Data Type	Data Provider	Data Date	Data Scale	Data Description
Digital Orthophoto	US Department of Agriculture	2010	*	NAIP Imagery
Digital Orthophoto	Coastal Services Center	2011	*	Coastal California LiDAR and digital imagery
Political boundaries	Santa Cruz County	2003	*	Municipal and county boundaries
Transportation Features	US Census Bureau	2009	*	2009 TIGER/Line shapefiles for Santa Cruz
Public Land Survey System (PLSS)	United States Geological Survey	1991	*	Public Lands Survey System linear features

Table 22: Base Map Sources

\*Data not available

#### 6.3 Floodplain and Floodway Delineation

The FIRM shows tints, screens, and symbols to indicate floodplains and floodways as well as the locations of selected cross sections used in the hydraulic analyses and floodway computations.

For riverine flooding sources, the mapped floodplain boundaries shown on the FIRM have been delineated using the flood elevations determined at each cross section; between cross sections, the boundaries were interpolated using the topographic elevation data described in Table 23. For each coastal flooding source studied as part of this FIS Report, the mapped floodplain boundaries on the FIRM have been delineated using the flood and wave elevations determined at each transect; between transects, boundaries were delineated using land use and land cover data, the topographic elevation data described in Table 23, and knowledge of coastal flood processes. In ponding areas, flood elevations were determined at each junction of the model; between junctions, boundaries were interpolated using the topographic elevation data described in Table 23.

In cases where the 1% and 0.2% annual chance floodplain boundaries are close together, only the 1% annual chance floodplain boundary has been shown. Small areas within the floodplain boundaries may lie above the flood elevations but cannot be shown due to limitations of the map scale and/or lack of detailed topographic data.

The floodway widths presented in this FIS Report and on the FIRM were computed for certain stream segments on the basis of equal conveyance reduction from each side of the floodplain. Floodway widths were computed at cross sections. Between cross sections, the floodway boundaries were interpolated. Table 2 indicates the flooding sources for which floodways have been determined. The results of the floodway computations for those flooding sources have been tabulated for selected cross sections and are shown in Table 24, "Floodway Data."

			Source	for Topograp	hic Elevation D	Data	
Community	Flooding Source	Description	Scale	Contour Interval	RMSEz	Accuracyz	Citation
Capitola, City of	Nobel Creek, Soquel Creek	Topographic Maps	1:600	2 ft	N/A	N/A	Ben B. White and Associates, Inc. 1965
Capitola, City of; Santa Cruz, City of; Santa Cruz County, Unincorporated Areas; Watsonville, City of	All riverine sources	Aerial Photography	1:4,800	4 ft	N/A	N/A	Spink Corp. 1978
Santa Cruz, City of	All riverine sources	Topographic Maps	1:1,200	4 ft	N/A	N/A	City of Santa Cruz 1974
Santa Cruz, City of; Santa Cruz County, Unincorporated Areas; Watsonville, City of	Pacific Ocean	LiDAR OPC / USGS 2009- 2011 & BATHY NOAA	N/A	2 ft	N/A	N/A	USGS 2009-2011
Santa Cruz County, Unincorporated Areas; Watsonville, City of	All riverine sources	Topographic Maps	1:1,200	2 ft	N/A	N/A	USACE 1971
Santa Cruz County, Unincorporated Areas	All Zone A sources	Topographic Maps	1;4,800	20 ft	N/A	N/A	Santa Cruz County 1965

 Table 23: Summary of Topographic Elevation Data used in Mapping

BFEs shown at cross sections on the FIRM represent the 1% annual chance water surface elevations shown on the Flood Profiles and in the Floodway Data tables in the FIS Report. Rounded whole-foot elevations may be shown on the FIRM in coastal areas, areas of ponding, and other areas with static base flood elevations.

	LOCATION		FLOODWAY		1% ANNU	AL CHANCE FLO ELEVATION (FE	OOD WATER SU EET NAVD88)	RFACE		
CRO SECT	SS ION DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/ SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE		
A B C D E F G H I J K	300 1,120 1,580 1,980 2,115 2,750 2,910 3,110 3,610 3,660 5,340 ve mouth at Pacific Oce	299 <sup>2</sup> 350 305 168 143 61 61 90 58 22 65 65	903 2,240 1,360 1,343 1,445 657 771 1,083 481 272 858	9.1 3.7 6.0 6.1 5.7 12.5 10.7 5.1 11.4 20.1 6.4	14.8 19.5 20.3 22.0 24.1 24.9 27.0 28.6 29.0 31.6 44.8	14.8 19.5 20.3 22.0 24.1 24.9 27.0 28.6 29.0 31.6 44.8	15.0 20.2 21.2 22.4 24.1 25.2 27.7 30.4 30.0 31.6 45.3	0.2 0.7 0.9 0.4 0.0 0.3 0.7 0.8 1.0 0.0 0.5		
FEDE		ANAGEMENT	AGENCY		FL	OODWAY	DATA			
SAN	TA CRUZ COUN AND INCORPORA	TY, CALII	ORNIA		FLOODING SOURCE: APTOS CREEK					

Table 24: Floodway Data

	LOCAT	ION		FLOODWAY		1% ANNU	AL CHANCE FLO ELEVATION (FE	DOD WATER SU ET NAVD88)	RFACE
CI SE	ROSS CTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
<sup>1</sup> Feet a	A B C D E F G H I J K L M N O	4,520 4,160 6,245 7,108 7,590 7,960 8,248 8,353 8,458 9,146 10,467 10,564 10,688 10,922 11,640 h at Pacific Oce	136 150 150 55 70 75 12 10 48 70 70 70 70 100 150	1,281 1,447 307 383 297 449 338 143 91 383 465 645 484 2,641 3,259 Bay)	$ \begin{array}{c} 1.2\\ 1.1\\ 5.1\\ 4.1\\ 5.3\\ 3.5\\ 4.6\\ 11.0\\ 17.2\\ 3.1\\ 2.6\\ 1.9\\ 2.5\\ 0.5\\ 0.4\\ \end{array} $	16.1 16.1 23.1 29.0 30.2 35.4 35.4 44.6 45.7 48.3 48.4 67.9 67.9	16.1 16.5 23.1 29.0 30.2 35.4 35.4 44.6 45.7 48.3 48.4 67.9 67.9	$ \begin{array}{c} 16.1\\ 16.5\\ 23.5\\ 29.2\\ 30.4\\ 36.0\\ 36.0\\ 36.0\\ 44.6\\ 46.1\\ 48.6\\ 48.9\\ 68.8\\ 68.8\\ 68.8\\ \end{array} $	$\begin{array}{c} 0.0\\ 0.0\\ 0.4\\ 0.2\\ 0.2\\ 0.6\\ 0.6\\ 0.6\\ 0.0\\ 0.4\\ 0.3\\ 0.5\\ 0.9\\ 0.9\\ \end{array}$
FE	EDERAL EN	IERGENCY MA	NAGEMENT	AGENCY		FL	.OODWAY I	ΟΑΤΑ	
SA		RUZ COUN <sup>-</sup> D INCORPORA	TY, CALIF ted areas	ORNIA		FLOODING	G SOURCE: A	RANA GULCI	4

LOCA	TION		FLOODWAY		1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATION (FEET NAVD88)				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
٨	50	50	470	0.0	24.4	24.4	24.4	0.0	
A	00	50	479	9.0	34.4	34.4	34.4	0.0	
В	115	102	550	7.9	34.7	34.7	34.7	0.0	
	980	86	652	0.0	38.2	38.2	38.2	0.0	
D	1,200	112	501	8.7	38.2	38.2	38.2	0.0	
E	2,540	/5	/44	5.8	42.8	42.8	42.8	0.0	
F	3,870	66	495	8.8	46.3	46.3	46.3	0.0	
G	4,970	65	373	11.6	55.6	55.6	55.6	0.0	
Н	6,020	81	468	9.3	68.8	68.8	68.8	0.0	
I	6,170	92	518	8.4	70.0	70.0	70.0	0.0	
J	6,400	118	1,694	2.6	89.3	89.3	89.3	0.0	
K	20,420	32	286	11.6	448.0	448.0	448.5	0.5	
L	21,530	35	280	11.9	465.8	465.8	466.1	0.3	
M	22,055	40	682	4.9	481.0	481.0	481.0	0.0	
Ν	22,430	50	512	5.3	481.3	481.3	481.4	0.1	
0	22,660	50	449	6.0	482.4	482.4	483.4	1.0	
Р	23,685	33	194	13.9	492.9	492.9	492.9	0.0	
Q	25,125	40	291	9.3	515.4	515.4	515.6	0.2	
R	26,595	54	261	10.3	542.9	542.9	542.9	0.0	
S	26,745	59	460	5.9	548.6	548.6	548.6	0.0	
T	27,720	130	642	3.8	552.8	552.8	553.4	0.6	
U	28,050	223	946	2.6	553.6	553.6	554.4	0.8	
eet above cor	fluence with Brand	ciforte Creek							
FEDERAL E	MERGENCY MA	NAGEMENT	AGENCY						
SANTA C	RUZ COUN	TY, CALII	ORNIA		FL	.00DWAY I			

AND INCORPORATED AREAS

	LOCATION		FLOODWAY		1% ANNU	AL CHANCE FLO	OOD WATER SU EET NAVD88)	RFACE	
CRO SECT	SS ION DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
V W Z AA AE AC AE AF AI AJ	29,055 30,065 30,265 31,995 32,305 33,790 33,790 33,790 33,775 33,785 33,785 33,785 33,785 33,785 33,785 33,790 33,77560 33,7,560 37,560 4,39,018 40,082 41,375	60 37 56 42 59 14 82 60 22 29 26 24 20 14 24 20 14 24	488 196 466 131 538 92 442 177 127 378 160 265 84 83 113	5.0 11.2 4.7 10.2 2.5 14.4 3.0 7.4 7.8 2.6 6.2 2.7 11.7 11.9 8.8	555.9 561.8 568.7 581.4 591.0 619.5 623.9 639.6 646.4 659.4 659.6 672.5 678.4 710.7 738.6	555.9 561.8 568.7 581.4 591.0 619.5 623.9 639.6 646.4 659.4 659.6 672.5 678.4 710.7 738.6	556.1 561.8 568.7 581.4 591.0 619.5 624.3 639.6 646.7 659.7 659.8 672.5 678.4 711.2 738.0	$\begin{array}{c} 0.2 \\ 0.0 \\ 0.0 \\ 0.0 \\ 0.0 \\ 0.0 \\ 0.4 \\ 0.0 \\ 0.3 \\ 0.2 \\ 0.0 \\ 0.0 \\ 0.5 \\ 0.6 \end{array}$	
FEDE	ERAL EMERGENCY M	ANAGEMENT	AGENCY		FL				
SAN		TY, CALIF		FLOODING SOURCE: CARBONERA CREEK					

LOCA	ΓΙΟΝ		FLOODWAY		1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATION (FEET NAVD88)				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE	
۸2	12 690	*	*	*	70.7	*	*	*	
A P <sup>2</sup>	13,080	*	*	*	70.7 75.6	*	*	*	
Б	15,050	111	024	0.5	75.0	01.2	01 0	0.5	
	17,410	144	1 106	9.5	85.5	85.5	86.2	0.5	
F	18 610	143	1,150	6.8	88.2	88.2	88.2	1.0	
F	21 090	109	765	10.0	00.2	00.2 00.6	00.2	0.0	
G	23,540	99	833	9.5	108 5	108 5	109.0	0.0	
н	23,680	97	853	9.0	110.3	110.3	110.9	0.0	
1	24 740	100	981	8.1	114.6	114.6	115.3	0.0	
J	24 880	88	997	8.0	115.4	115.4	115.8	0.4	
ĸ	28.310	215	1.377	5.8	127.4	127.4	127.4	0.0	
L	28.430	212	1.475	5.4	128.0	128.0	128.0	0.0	
M	29.450	128	889	8.9	130.8	130.8	131.5	0.7	
Ν	31.850	98	820	9.7	142.2	142.2	143.2	1.0	
0	33,360	200	950	8.4	152.5	152.5	152.8	0.3	
Р	33,480	200	1,046	7.6	153.0	153.0	153.6	0.6	
Q	35,910	144	982	8.1	161.0	161.0	161.3	0.3	
R	37,630	80	894	8.9	169.3	169.3	169.9	0.6	
S	40,310	96	750	10.6	185.3	185.3	185.4	0.1	
Т	40,480	139	1,546	5.1	193.6	193.6	193.6	0.0	
U	41,830	85	790	10.0	195.5	195.5	196.0	0.5	
V	43,910	107	1,065	7.5	206.9	206.9	207.4	0.5	

<sup>1</sup>Feet above confluence with Pajaro River

TABLE

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<sup>2</sup>Floodway not computed/shown for this cross section

### FEDERAL EMERGENCY MANAGEMENT AGENCY

## SANTA CRUZ COUNTY, CALIFORNIA

AND INCORPORATED AREAS

## FLOODWAY DATA

#### FLOODING SOURCE: CORRALITOS CREEK

LOCA	TION		FLOODWAY		1% ANNU	AL CHANCE FLO ELEVATION (FE	DOD WATER SU ET NAVD88)	RFACE		
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE		
W X Y Z AA AB AC	45,970 47,610 48,250 49,430 49,560 51,650 52,550	102 80 100 113 119 87 93	1,019 537 862 860 655 564 829	7.8 14.8 9.2 9.2 12.1 14.1 9.6	218.8 225.2 233.6 241.0 243.0 256.4 267.3	218.8 225.2 233.6 241.0 243.0 256.4 267.3	219.8 225.2 234.1 241.4 243.0 256.5 267.3	1.0 0.0 0.5 0.4 0.0 0.1 0.0		
FEDERAL I		ANAGEMENT	AGENCY		FL					
SANTA C	RUZ COUN	TY, CALII	FORNIA		FLOODING SOURCE: CORRALITOS CREEK					

LO	CATION		FLOODWAY		1% ANNU	AL CHANCE FLO ELEVATION (FE	OOD WATER SU EET NAVD88)	RFACE
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A <sup>2</sup> B <sup>2</sup> C <sup>2</sup> D <sup>2</sup> E <sup>2</sup> F <sup>2</sup>	1,314 1,446 2,590 4,869 4,992 5,460 onfluence with Pajar computed for this str	* * * * o River eam	* * * * * *	* * * * * *	42.3 42.7 44.5 44.6 44.7	* * * * * *	* * * * * *	* * * * *
FEDERA			AGENCY		FL	OODWAY	DATA	
SANTA	AND INCORPORA	TY, CALII	-ORNIA	FLC		CE: COWARD	CREEK/LAK	E TYNAN

LOCA	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD V (FEET N/	1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATION (FEET NAVD88)				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE			
A B C D E F G H I J K L M N	780 3,040 3,460 5,320 7,970 8,360 11,220 13,360 13,640 13,850 14,540 16,580 17,530 18,670	706 120 201 350 411 422 401 139 150 100 108 125 101 81	2,889 864 1,733 2,847 2,729 2,954 2,566 397 631 379 1,586 1,187 638 242	0.8 2.7 1.3 0.8 0.7 0.6 0.7 4.5 2.8 4.7 1.1 1.5 2.8 7.3	16.8 16.8 16.8 16.8 16.8 16.8 16.8 16.8	$\begin{array}{c} 8.7^2 \\ 9.0^2 \\ 10.4^2 \\ 10.4^2 \\ 10.4^2 \\ 10.5^2 \\ 11.7^2 \\ 13.5^2 \\ 13.6^2 \\ 28.5 \\ 28.6 \\ 28.7 \\ 34.1 \end{array}$	$\begin{array}{c} 9.5^2 \\ 9.7^2 \\ 11.2^2 \\ 11.3^2 \\ 11.3^2 \\ 11.5^2 \\ 12.4^2 \\ 14.0^2 \\ 14.1^2 \\ 28.5 \\ 28.7 \\ 29.0 \\ 34.1 \end{array}$	$\begin{array}{c} 0.8\\ 0.7\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 1.0\\ 0.7\\ 0.5\\ 0.5\\ 0.0\\ 0.1\\ 0.3\\ 0.0\\ \end{array}$			
<sup>1</sup> Feet above confl <sup>2</sup> Elevation comput FEDERAL I SANTA C	uence with Watsor ted without conside EMERGENCY MA CRUZ COUN	NVIIIE Slough Peration of back NAGEMENT TY, CALII TED AREAS	AGENCY	m Pajaro River	FLOODING	OODWAY SOURCE: HA	DATA RKINS SLOUG	) SH			
	LOCAT	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION		
----------	--	---	--	--	---	--	--	--	---		
	CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE		
	A B C D E F G H I I	410 1,310 1,610 2,250 4,657 4,854 5,059 5,424 6,077	90 80 70 60 50 109 8 30 30 30	128 330 100 236 170 1,278 92 335 173	5.0 1.9 6.3 2.7 3.7 0.5 6.9 1.9 3.7	10.9 12.5 14.2 20.9 43.5 57.6 57.6 61.1 61.1	10.9 12.5 14.2 20.9 43.5 57.6 57.6 61.1 61.1	11.1 13.5 14.4 21.9 44.5 57.6 57.6 61.1 62.0	0.2 1.0 0.2 1.0 1.0 0.0 0.0 0.0 0.9		
<u>۲</u>	FEDERAL E	MERGENCY MA	NAGEMENT	AGENCY		FI		ΠΔΤΔ			
BIF 24	SANTA C	RUZ COUN	TY, CALIF	ORNIA		FLOODING	G SOURCE: M	OORE CREEK	(		

	LOCAT	ION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
	CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
	A B C D E F	1,700 2,820 2,820 4,137 4,374 5,014	89 30 17 30 22	861 295 321 55 188 59	0.6 1.9 1.7 10.2 3.0 9.4	51.6 56.7 64.7 72.6 77.8	51.6 56.7 64.7 72.6 77.8	52.6 57.7 64.7 72.6 77.8	1.0 1.0 0.0 0.0 0.0
	<sup>1</sup> Feet above conflue	ence with Soquel	Creek	<u> </u>	<u> </u>	<u> </u>			<u> </u>
TAE	FEDERAL EI	MERGENCY MA		AGENCY		FL	OODWAY	DATA	
3LE 24	SANTA CI	RUZ COUN	TY, CALIF ted areas	ORNIA		FLOODIN	G SOURCE: N	OBEL CREEK	

CROSS SECTION	DISTANCE <sup>1</sup>					(FEET NA	VD88)	
٨		(FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
С В С D Е F G H <sup>4</sup> J <sup>4</sup> K <sup>4</sup> L <sup>4</sup> N <sup>4</sup> P <sup>4</sup>	200 2,840 7,680 10,440 13,101 13,219 15,760 18,120 20,278 20,883 23,020 26,940 28,500 29,899 30,031 31,095	1,535 <sup>2</sup> 4,570 3 3 3 3 * * * * * * *	4,419 27,409 3 3 3 3 * * * * * * *	9.9 1.6 3 3 3 * * * * * *	* 15.1 18.3 20.6 22.5 22.5 24.2 26.1 29.5 30.1 30.6 35.8 37.0 38.4 38.4 38.4 38.4	11.4 15.1 18.3 20.6 22.5 24.2 * * * * * *	11.4 15.1 3 3 3 * * * * * * * * *	0.0 0.0 3 3 3 3 3 * * * * * * * * *
<sup>1</sup> Feet above mouth <sup>2</sup> Width includes area <sup>3</sup> Floodway compute <sup>4</sup> Floodway not comp *Controlled by coas FEDERAL EN	at Pacific Ocean a of coastal veloc d without consid buted/shown for tal flooding – see	city hazards eration of levee this cross sect Flood Insurar NAGEMENT	e ion nce Rate map fo AGENCY	r regulatory base	flood elevation	OODWAY	DATA	

AND INCORPORATED AREAS

ELEVATION	ATER SURFACE VD88)	IANCE FLOOD W (FEET NA	1% ANNUAL CH		FLOODWAY		ΓΙΟΝ	LOCA
INCREASE	WITH FLOODWAY	WITHOUT FLOODWAY	REGULATORY	MEAN VELOCITY (FEET/SEC)	SECTION AREA (SQ. FEET)	WIDTH (FEET)	DISTANCE <sup>1</sup>	CROSS SECTION
*	*	*	38.8	*	*	*	31 285	$O^3$
*	*	*	40 3	*	*	*	34 575	R <sup>3</sup>
*	*	*	42.2	*	*	*	36 240	S <sup>3</sup>
*	*	*	44.5	*	*	*	38,560	$T^3$
*	*	*	44.9	*	*	*	39,440	U <sup>3</sup>
*	*	*	47.2	*	*	*	43,100	$V^3$
2	2	50.5	50.5	2	2	2	46,145	Ŵ
2	2	53.0	53.0	2	2	2	48,395	Х
2	2	57.0	57.0	2	2	2	52,015	Y
2	2	59.6	59.6	2	2	2	54,105	Z
2	2	62.5	62.5	2	2	2	57,665	AA
2	2	64.9	64.9	2	2	2	60,610	AB
2	2	64.9	64.9	2	2	2	60,850	AC
0.0	65.5	65.5	65.5	5.5	7,784	1,340 <sup>4</sup>	62,270	AD
0.5	68.7	68.2	68.2	10.4	4,152	300 <sup>4</sup>	66,110	AE
07	72.0	71.3	71.3	10.5	4,099	300 <sup>4</sup>	68,240	AF

<sup>1</sup>Feet above mouth at Pacific Ocean

<sup>2</sup>Floodway computed without consideration of levee

<sup>3</sup>Floodway not computed/shown for this cross section

<sup>4</sup>Width extends beyond county boundary

#### FEDERAL EMERGENCY MANAGEMENT AGENCY

# TABLE 24

## SANTA CRUZ COUNTY, CALIFORNIA

#### AND INCORPORATED AREAS

## FLOODWAY DATA

#### FLOODING SOURCE: PARAJO RIVER

LOCA	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
AG AH AJ AK AL AM	71,020 73,820 76,380 79,237 79,362 82,020 84,440	304 <sup>2</sup> 271 <sup>2</sup> 500 <sup>2</sup> 393 <sup>2</sup> 447 <sup>2</sup> 500 <sup>2</sup> 203 <sup>2</sup>	6,052 5,392 6,064 6,471 6,155 4,337 3,756	7.1 7.6 7.1 6.6 7.0 9.5 11.4	77.2 80.6 82.7 85.5 85.6 87.5 91.9	77.2 80.6 82.7 85.5 85.6 87.5 91.9	77.5 80.9 83.2 86.1 86.1 88.5 92.5	0.3 0.5 0.6 0.5 1.0 0.6
<sup>1</sup> Feet above mout <sup>2</sup> Width extends be	h at Pacific Ocean eyond county boun	dary						
FEDERAL					FL	OODWAY	DATA	
SANIAC		IT, CALIF	UKNIA		FLOODIN	G SOURCE: P	ARAJO RIVER	

ELEVATIO	ATER SURFACE	ANCE FLOOD W (FEET NA	1% ANNUAL CH		FLOODWAY		TION	LOCA
INCREAS	WITH FLOODWAY	WITHOUT FLOODWAY	REGULATORY	MEAN VELOCITY (FEET/SEC)	SECTION AREA (SQ. FEET)	WIDTH (FEET)	DISTANCE <sup>1</sup>	CROSS SECTION
0.0	15.1	15.1	15.1	1.6	27,409	4,570	2,840	A
0.2	15.9	15.7	15.7	2.0	21,892	5,116	7,680	В
0.6	16.8	16.2	16.2	1.5	28,165	5,488	10,440	С
0.8	17.4	16.6	16.6	1.5	28,665	5,350	13,101	D
0.8	17.5	16.7	16.7	1.5	29,269	5,315	13,219	E
0.8	17.9	17.1	17.1	1.4	30,289	5,422	15,760	F
*	*	*	17.3	*	*	*	18,120	G <sup>2</sup>
*	*	*	17.4	*	*	*	20,278	$H^2$
*	*	*	22.6	*	*	*	20,883	$ ^2$
*	*	*	23.1	*	*	*	23,020	$J^2$
*	*	*	25.7	*	*	*	26,940	K <sup>2</sup>
*	*	*	26.8	*	*	*	28,500	L <sup>2</sup>
1.0	46.8	45.8	45.8	2.3	18,408	3,683	46,145	М
0.8	47.9	47.1	47.1	3.1	13,953	2,700	48,395	Ν
0.3	51.2	50.9	50.9	4.3	10,093	2,200	52,015	0
0.7	53.3	52.6	52.6	4.0	10,804	2,100	54,105	Р
0.8	56.4	55.6	55.6	3.9	11,024	2,400	57,665	Q
0.3	59.9	59.6	59.6	4.9	8,709	1,375	60,610	R
0.0	60.9	60.9	60.9	4.3	9.916	1.320	60.850	S

<sup>1</sup>Feet above mouth at Pacific Ocean

TABLE

24

<sup>2</sup>Floodway not computed/shown for this cross section

FEDERAL EMERGENCY MANAGEMENT AGENCY

## SANTA CRUZ COUNTY, CALIFORNIA

#### AND INCORPORATED AREAS

## FLOODWAY DATA

FLOODING SOURCE: PARAJO RIVER-WITHOUT LEVEE CONSIDERATION

LOCA	TION		FLOODWAY	1	1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A B C D E F G H – J K L M N O	$\begin{array}{c} 750\\ 2,505\\ 3,020\\ 4,550\\ 4,670\\ 5,220\\ 5,440\\ 6,225\\ 6,960\\ 7,180\\ 9,205\\ 10,385\\ 10,945\\ 12,565\\ 14,255\end{array}$	200 148 40 68 68 68 70 70 30 49 47 120 40 40 40	1,540 253 369 309 237 420 776 423 121 1,060 325 389 748 345 280	1.0 6.1 4.2 5.0 6.5 3.3 1.8 3.3 11.5 1.3 3.8 3.2 1.6 3.1 3.8	$10.5 \\ 10.6 \\ 16.9 \\ 21.5 \\ 22.2 \\ 24.7 \\ 29.6 \\ 29.7 \\ 33.6 \\ 56.1 \\ 56.5 \\ 62.6 \\ 81.4 \\ 81.5 \\ 83.3 \\$	$10.5 \\ 10.6 \\ 16.9 \\ 21.5 \\ 22.2 \\ 24.7 \\ 29.6 \\ 29.7 \\ 33.6 \\ 56.1 \\ 56.5 \\ 62.6 \\ 81.4 \\ 81.5 \\ 83.3 \\$	10.5 10.7 17.7 21.6 22.9 25.5 29.7 30.0 33.7 56.1 57.0 63.6 81.4 81.8 84.1	$\begin{array}{c} 0.0\\ 0.1\\ 0.8\\ 0.1\\ 0.7\\ 0.8\\ 0.1\\ 0.3\\ 0.1\\ 0.0\\ 0.5\\ 1.0\\ 0.0\\ 0.3\\ 0.8\end{array}$
eet above mout	h							

## SANTA CRUZ COUNTY, CALIFORNIA

TABLE 24

AND INCORPORATED AREAS

## FLOODWAY DATA

## FLOODING SOURCE: RODEO CREEK GULCH

LOCAT	ION		FLOODWAY	-	1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A B C D E <sup>3</sup> G <sup>3</sup> H <sup>3</sup> J <sup>3</sup> J <sup>3</sup>	870 1,070 3,170 5,592 6,400 7,820 9,310 12,010 12,610 13,480 ence with Pajaro	95 96 213 139 * * * * * * *	962 995 1,230 990 * * * * *	6.2 6.0 4.8 6.0 * * * * * *	39.8 39.8 41.7 47.0 49.2 51.9 58.8 64.8 65.8 70.7	35.7 <sup>2</sup> 36.1 <sup>2</sup> 41.7 47.0 * * *	35.7 <sup>2</sup> 36.1 <sup>2</sup> 42.1 47.4 * * *	0.0 0.4 0.4 * * * *
"No floodway comp FEDERAL E	MERGENCY MA		AGENCY					
SANTA C		TY, CALIF	ORNIA		FL	OODWAY	DATA	
A	ND INCORPORA	TED AREAS			FLOODING S	OURCE: SALS	SIPUEDES CR	EEK

	LOCAT	ION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
	CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
	C D F G	3,170 5,592 6,400 7,820 9,310	* * * *	2 2 2 2 2	2 2 2 2 2	41.7 46.1 46.4 49.9 58.8	41.7 46.1 46.4 49.9 58.8	2 2 2 2	2 2 2 2 2
	<sup>2</sup> Floodway compute	ed with considera	ation of levee						
	FEDERAL E					FL	OODWAY	DATA	
1	SANTA CI AN	NUZ COUN	TED AREAS	UKNIA	FLO	ODING SOURC	E: SALSIPUE	DES CREEK- LEFT LEVEE	WITHOUT

	LOCATION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
CRO SECT	SS ION DISTANCI	<sup>1</sup> WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A B C D	870 1,070 3,220 5,330	* * *	2 2 2 2 2	2 2 2 2 2	34.4 34.7 40.1 42.6	34.4 34.7 40.1 42.6	2 2 2	2 2 2 2
<sup>1</sup> Feet abov <sup>2</sup> Floodway	ve confluence with Paj v computed with consid	aro River deration of levee						
FED		MANAGEMENT	AGENCY		FL	OODWAY	DATA	
SAN	ITA CRUZ COU AND INCORPO	JNTY, CALIF PRATED AREAS	FORNIA	FLO	ODING SOURC	E: SALSIPUE	DES CREEK- V RIGHT LEVEE	WITHOUT

LOCA	TION		FLOODWAY		1% ANNUAL CH	ANCE FLOOD W	ATER SURFACE	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
•	020	2	2	2	12.0	12.0	2	2
A	938	2	2	2	13.0	13.0	2	2
В	1,062	2	2	2	13.1	13.1	2	2
	1,812	2	2	2	14.2	14.2	2	2
D	2,952	2	2	2	15.8	15.8	2	2
E	3,354	- 2	2	2	16.9	16.9	2	2
F	4,559	- 2	2	2	20.6	20.6	2	- 2
G	4,745	2	2	2	21.0	21.0	2	2
Н	5,933	2	2	2	23.8	23.8	2	2
I	6,099	2	2	2	24.1	24.1	2	2
J	7,686	2	2	2	25.2	25.2	2	2
K	7,948	2	2	2	27.2	27.2	2	2
L	9,303	2	2	2	28.0	28.0	2	2
Μ	10,388	2	2	2	28.7	28.7	2	2
Ν	10,677	400	5,148	9.2	30.3	30.3	30.3	0.0
0	11,991	399	5,194	9.2	32.6	32.6	32.6	0.0
Р	13,016	400	5,431	8.5	34.3	34.3	34.3	0.0
Q	16,428	260	3,184	14.6	39.9	39.9	40.6	0.7
R	17,903	237	3,347	13.9	45.5	45.5	45.7	0.2
S	18,578	246	5,248	8.8	51.6	51.6	51.6	0.0
Т	19,558	234	3,133	14.8	51.8	51.8	52.0	0.2
U	20,898	240	3,097	13.0	57.4	57.4	58.0	0.6
V	21.828	233	4.326	10.7	63.6	62.8	64.2	1.4
W	23,088	234	3,963	11.7	65.8	65.8	66.8	1.0
-eet above mout	h at Pacific Ocean	(Monterey Ba	y)					
Floodway compu	ited without consid	eration of leve	e					
FEDERAL I	EMERGENCY MA	NAGEMENT	AGENCY					
SANTA C					FL	UUDWAT		
Δ		TED AREAS			FLOODING S	OURCE: SAN		/ER

ELEVATION	ATER SURFACE	ANCE FLOOD W (FEET NA	1% ANNUAL CH		FLOODWAY		TION	LOCA
INCREASE	WITH FLOODWAY	WITHOUT FLOODWAY	REGULATORY	MEAN VELOCITY (FEET/SEC)	SECTION AREA (SQ. FEET)	WIDTH (FEET)	DISTANCE <sup>1</sup>	CROSS SECTION
0.0	<u> </u>	<u> </u>	<u> </u>	40.0	2.047	457	00,400	V
0.6	69.4	68.8 70.7	68.8 70.7	12.2	3,817	157	23,408	X
0.9	71.6	70.7	70.7	16.2	2,864	156	25,078	ř Z
0.0	259.2	259.2	259.2	6.5 0.5	6,592	452	43,599	Ζ
0.0	262.2	202.2	262.2	2.5	7,448	800	45,739	AA
0.6	263.5	262.9	262.9	3.9	11,078	1,000	48,726	AB
0.5	263.7	263.2	263.2	4.2	1,083	1,000	48,982	AC
0.7	264.4	263.7	263.7	3.7	11,673	1,000	49,281	AD
0.8	264.9	264.1	264.1	3.4	12,667	1,000	49,673	AE
0.9	266.7	265.8	265.8	4.2	8,666	786	52,365	AF
0.7	266.7	266.0	266.0	7.8	4,670	481	52,640	AG
1.0	268.3	267.3	267.3	8.4	4,353	241	53,321	AH
0.8	269.1	268.3	268.3	9.2	3,968	178	53,455	AI
0.1	269.3	269.2	269.2	16.9	2,164	156	54,713	AJ
0.0	278.0	278.0	278.0	12.0	3,033	137	55,783	AK
0.0	281.3	281.3	281.3	10.9	3,349	134	57,098	AL
0.0	286.7	286.7	286.7	7.1	4,801	205	60,048	AM
0.0	288.1	288.1	288.1	11.7	2,900	160	61,998	AN
0.0	291.1	291.1	291.1	10.6	3,203	174	62,128	AO
0.0	292.4	292.4	292.4	11.0	3,091	163	63,265	AP
0.0	296.6	296.6	296.6	10.0	3,386	163	63,502	AQ
0.0	298.4	298.4	298.4	10.9	3,127	159	65,308	AR
0.4	305.5	305.1	305.1	9.0	3,784	153	67,988	AS

eet above mouth at Pacific Ocean (Monterey bay)

TABLE

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FEDERAL EMERGENCY MANAGEMENT AGENCY

## **FLOODWAY DATA**

SANTA CRUZ COUNTY, CALIFORNIA AND INCORPORATED AREAS

#### FLOODING SOURCE: SAN LORENZO RIVER

CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
AT	68,095	153	3,835	8.9	305.4	305.4	305.8	0.4
AU	69,173	188	3,156	10.8	305.9	305.9	306.4	0.5
AV	70,113	309	6,000	5.7	310.0	310.0	310.0	0.0
AW	72,818	106	1,982	15.0	312.4	312.4	312.7	0.3
AX	75,455	258	4,380	6.3	321.8	321.8	321.9	0.1
AY	75,592	166	3,527	7.8	323.1	323.1	323.1	0.0
AZ	75,890	169	3,541	7.8	324.2	324.2	324.2	0.0
BA	76,087	186	2,478	11.0	324.2	324.2	324.3	0.1
BB	77,411	114	1,522	18.2	327.4	327.4	327.4	0.0
BC	77,548	124	1,949	14.2	334.1	334.1	334.1	0.0
BD	79,844	171	2,203	12.2	340.6	340.6	340.6	0.0
BE	81,084	183	1,898	14.2	348.0	348.0	348.2	0.2
BF	83,293	122	1,999	13.5	366.7	366.7	367.7	1.0
BG	83,515	124	2,103	12.8	370.0	370.0	370.0	0.0
BH	84,779	168	2,139	12.6	374.4	374.4	374.5	0.1
BI	86,227	110	1,806	14.3	384.1	384.1	384.1	0.0
BJ	86,342	114	1,958	13.2	387.0	387.0	387.0	0.0
BK	88,429	118	1,835	14.1	393.6	393.6	393.6	0.0
BL	89,273	121	1,338	19.3	400.0	400.0	400.2	0.2
BM	89,585	195	2,163	11.9	406.6	406.6	406.6	0.0
BN	92,159	181	3,225	7.5	418.2	418.2	418.2	0.0
BO	93,351	159	2,011	12.0	419.1	419.1	419.1	0.0
BP	93,517	151	2,355	10.2	423.7	423.7	423.7	0.0

## FLOODWAY DATA

SANTA CRUZ COUNTY, CALIFORNIA

TABLE 24

AND INCORPORATED AREAS

FLOODING SOURCE: SAN LORENZO RIVER

LOCA	TION		FLOODWAY		1% ANNUAL CH	ANCE FLOOD W	ATER SURFACE	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
BO	95 354	168	1 851	13.0	427 7	426.8	427 8	1.0
BR	97 474	139	2 355	10.0	441.8	441 8	441.8	0.0
BS	99,559	146	1 708	14 1	447.0	441.0 447 4	447.6	0.0
BT	100 846	180	2 343	10.3	458.4	458.4	458.4	0.0
BU	100,976	180	3,339	74	462.7	462.7	462.7	0.0
BV	102,626	85	1,370	89	464.9	464.9	465.7	0.8
BW	103,736	99	1,825	6.7	468.2	468.2	468.6	0.4
BX	104,956	62	921	13.2	469.0	469.0	469.4	0.4
BY	105,176	64	1.062	11.5	471.3	471.3	471.8	0.5
BZ	108.646	67	729	16.7	482.4	482.4	482.4	0.0
ĊĂ	109.377	96	1,483	8.2	490.9	490.9	490.9	0.0
CB	109,595	103	1,577	7.7	494.5	494.5	494.5	0.0
CC	111,766	127	1,793	5.9	499.4	499.4	499.4	0.0
CD	112,766	58	670	15.7	500.2	500.2	500.2	0.0
CE	112,886	63	859	12.3	502.9	502.9	502.9	0.0
CF	113,526	140	2,062	5.1	506.5	506.5	506.5	0.0
CG	113,651	138	1,880	5.6	506.5	506.5	506.5	0.0
СН	114,573	103	1,025	10.3	508.6	508.6	508.7	0.1
CI	114,789	91	1,132	9.3	510.7	510.7	510.8	0.1
CJ	118,356	135	1,415	4.3	522.3	522.3	522.8	0.5
СК	121,138	96	861	7.1	536.3	536.3	536.3	0.0
CL	121,264	92	1,025	6.0	538.5	538.5	538.5	0.0
CM	122,516	97	621	9.9	543.9	543.9	543.9	0.0

TABLE 24

## SANTA CRUZ COUNTY, CALIFORNIA

#### AND INCORPORATED AREAS

## FLOODWAY DATA

#### FLOODING SOURCE: SAN LORENZO RIVER

	LOCATION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE VD88)	ELEVATION
CROS SECTIO	S DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
CN CO CP CQ CR CS CT CU CV CW CV CW CZ DA DB DC DD DE DG DH	123,862 123,973 125,349 125,495 126,980 127,145 127,570 127,735 128,659 128,825 130,517 131,197 132,261 132,442 133,499 134,459 137,442 138,233 138,355 140,439 141,389	95 95 56 58 34 56 47 52 55 74 69 51 40 66 63 48 49 34 50 55 42	1,139 1,117 480 560 386 535 497 542 750 741 447 347 511 732 344 408 318 257 343 313 330	$\begin{array}{c} 5.4\\ 5.5\\ 12.8\\ 11.0\\ 14.4\\ 10.4\\ 11.2\\ 10.3\\ 7.4\\ 7.5\\ 11.2\\ 14.5\\ 8.3\\ 5.8\\ 12.3\\ 10.4\\ 13.3\\ 16.5\\ 12.3\\ 13.5\\ 12.8\\ \end{array}$	550.2 550.3 554.0 556.0 563.6 567.6 569.6 571.0 575.0 575.0 582.7 594.5 603.4 609.0 612.8 623.5 644.1 656.3 661.2 678.5 690.6	550.2 550.3 554.0 563.6 567.6 569.6 571.0 575.0 575.0 582.7 594.5 603.4 609.0 612.8 623.5 644.1 659.3 661.2 678.5 690.6	$\begin{array}{c} 550.2\\ 550.3\\ 553.8\\ 556.0\\ 564.5\\ 567.6\\ 569.6\\ 571.0\\ 575.6\\ 575.8\\ 582.7\\ 594.5\\ 603.9\\ 609.1\\ 612.9\\ 623.5\\ 644.1\\ 656.4\\ 661.2\\ 678.3\\ 691.3\end{array}$	$\begin{array}{c} 0.0\\ 0.0\\ 0.2\\ 0.0\\ 0.9\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.6\\ 0.8\\ 0.0\\ 0.0\\ 0.5\\ 0.1\\ 0.1\\ 0.1\\ 0.1\\ 0.0\\ 0.0\\ 2.9\\ 0.0\\ 0.2\\ 0.7\\ \end{array}$
<sup>1</sup> Feet above	e mouth at Pacific Ocean	(Monterey Ba						
SAN	TA CRUZ COUN	TY, CALIF	ORNIA		FL	OODWAY		(55)
	AND INCORPORA	TED AREAS			FLOODING S	OURCE: SAN	LORENZO RIV	/EK

LOCA	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE VD88)	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A B C D E F G H I J K L M	938 1,062 1,812 2,952 3,354 4,559 4,745 5,933 6,099 7,686 7,948 9,303 10,388	288 286 319 997 983 1,975 1,930 875 989 346 288 330 299	4,021 3,919 4,336 8,300 9,424 9,205 11,165 5,299 7,757 4,206 4,550 4,028 4,081	12.6 12.9 11.7 6.1 5.4 5.5 4.5 9.5 6.5 11.3 10.5 11.8 11.7	13.0 13.1 14.2 15.8 16.6 17.5 18.3 18.8 20.0 22.9 24.3 26.1 26.7	13.0 13.1 14.2 15.8 16.6 17.5 18.3 18.8 20.0 22.9 24.3 26.1 26.7	13.0 13.1 14.2 15.8 16.6 17.5 18.7 19.4 21.0 23.1 24.4 26.1 27.7	0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.6 1.0 0.2 0.1 0.0 1.0
<sup>1</sup> Feet above mouth	at Pacific Ocean							
FEDERAL E					FL	OODWAY	DATA	
SANTA C	NUZ COUN	TED AREAS	OKNIA	FLOOD	ING SOURCE:	SAN LORENZO CONSIDERAT	O RIVER- WITI TION	HOUT LEVE

LOG	ATION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	VATER SURFACE AVD88)	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A B C D E F G H I I	300 675 1,035 1,735 1,975 2,475 2,955 3,575 4,475 vuth at Pacific Ocean coastal flooding – se	36 15 63 70 83 359 152 129 205 205	212 219 1,132 517 535 526 412 384 517 nce Rate Map fo	13.5 13.1 2.5 5.5 5.3 5.4 6.9 7.4 5.5 7.4 5.5	* 21.6 31.0 31.1 31.6 36.8 43.9 55.0 69.0 flood elevation	12.4 21.6 31.0 31.1 31.6 36.8 43.9 55.0 69.0	12.4 21.6 31.0 31.3 32.3 36.8 43.9 55.0 69.0	0.0 0.0 0.2 0.7 0.0 0.0 0.0 0.0 0.0
FEDERA	L EMERGENCY MA	NAGEMENT	AGENCY		FL	OODWAY	DATA	
SANTA	CRUZ COUN	TY, CALIF	ORNIA		FLOODING S	OURCE: SAN	VICENTE CRE	EEK

	LOCAT	ION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
	CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
	A <sup>2</sup> B <sup>2</sup> C <sup>2</sup> <sup>1</sup> Feet above mouth <sup>2</sup> No floodway comp	480 540 2,200	* * *	* * *	* * *	3 3 3	* * *	* *	* * *
TAB	FEDERAL E	MERGENCY MA	NAGEMENT	AGENCY		FL	OODWAY	DATA	
LE 24		RUZ COUN' ND INCORPORA	TY, CALIF ted areas	ORNIA		FLOODING S	SOURCE: SCH		ON

CROSS SECTION	DISTANCE1	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
۸	220	504	4 000	0.2	445		445	0.0
A	220	591	1,882	9.3	14.5	14.5	14.5	0.0
В	470	372	2,536	6.9	17.0	17.0	17.0	0.0
	720	340	3,007	5.8	18.9	18.9	18.9	0.0
D	1,120	300	3,614	4.8	19.5	19.5	19.6	0.1
E	2,330	105	1,170	14.8	19.6	19.6	19.6	0.0
F	3,250	142	1,940	8.9	25.7	25.7	25.7	0.0
G	4,720	162	2,290	7.6	30.6	30.6	30.7	0.1
н	5,100	1/1	2,130	8.1	33.9	33.9	34.5	0.6
I	5,970	355	3,140	5.5	36.9	36.9	37.8	0.9
J	6,115	487	4,200	4.1	39.5	39.5	40.1	0.6
K	8,140	600	4,770	3.6	42.6	42.6	43.3	0.7
L	8,385	623	6,770	2.6	44.4	44.4	45.3	0.9
М	9,355	106	1,190	14.6	44.4	44.4	45.3	0.9
N	11,235	236	3,050	5.7	54.9	54.9	55.1	0.2
0	13,915	301	2,520	6.5	59.7	59.7	60.6	0.9
Р	18,435	179	2,060	8.0	81.9	81.9	82.4	0.5
Q	21,995	161	1,680	9.7	99.7	99.7	99.7	0.0
R	24,835	266	1,600	10.2	108.8	108.8	108.8	0.0
S	25,835	470	4,160	3.9	115.1	115.1	115.1	0.0
Т	26,555	280	2,100	7.8	116.4	116.4	116.4	0.0
U	27,755	155	1,260	13.0	123.3	123.3	123.3	0.0
V	29,025	120	1,300	11.8	134.9	134.9	135.0	0.1
W	29,310	153	2,260	6.8	143.9	143.9	143.9	0.0

## FLOODWAY DATA

SANTA CRUZ COUNTY, CALIFORNIA

TABLE 24

AND INCORPORATED AREAS

FLOODING SOURCE: SOQUEL CREEK

LOCA	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE VD88)	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
X Y Z AA AB AC AD AE <sup>1</sup> Feet above mout	32,500 32,970 33,085 34,825 36,825 38,025 38,135 39,735	154 93 92 132 141 108 114 110	1,780 1,070 1,420 2,290 1,820 1,390 1,610 1,742	8.6 14.2 10.8 6.7 8.4 11.0 9.5 8.8	154.1 157.4 161.8 171.7 178.0 189.0 191.5 199.0	154.1 157.4 161.8 171.7 178.0 189.0 191.5 199.0	155.1 157.4 161.9 172.7 179.0 189.0 191.5 199.4	1.0 0.0 0.1 1.0 1.0 0.0 0.0 0.4
FEDERAL	EMERGENCY MA	NAGEMENT	AGENCY					
SANTA (		TY, CALIF	ORNIA		FL	UUDWAY	DATA	
Δ				FLOODING	SOURCE: SO		κ	

LOCA	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	/ATER SURFACE AVD88)	ELEVATION
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A B C D E F G H I J K L M N	800 1,700 1,830 3,130 4,560 5,840 5,980 6,086 7,071 8,511 9,587 10,419 12,994 13,178	351 143 102 158 100 81 123 205 86 310 212 179 16 50	874 403 409 325 305 313 266 1,145 93 4,989 2,888 1,314 34 60	0.8 1.7 1.7 2.2 1.4 1.4 1.6 0.5 5.9 0.1 0.2 0.2 9.2 5.2	17.4 17.4 17.4 17.4 17.4 17.4 17.4 17.4	$6.4^2$ $6.6^2$ $7.0^2$ $7.7^2$ $9.2^2$ $9.6^2$ $9.7^2$ $9.6^2$ $12.9^2$ 25.5 25.5 25.5 53.6 57.5	7.4 7.5 7.9 8.7 10.1 10.6 10.6 10.2 12.9 26.4 26.4 26.4 26.4 26.4 53.7 57.6	$ \begin{array}{c} 1.0\\ 0.9\\ 0.9\\ 1.0\\ 0.9\\ 1.0\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.1\\ 0.1\\ \end{array} $
Elevation compu	ted without conside	eration of back	water effects fror	m Pajaro River				
FEDERAL	EMERGENCY MA				FL	OODWAY	DATA	
	ND INCORPORA	TED AREAS			FLOODING	SOURCE: ST	RUVE SLOUG	H

	LOCAT	ION		FLOODWAY		1% ANNUAL CH			ELEVATION
	CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
	A <sup>2</sup> B <sup>2</sup> C <sup>2</sup> D <sup>2</sup> E <sup>2</sup>	1,040 2,080 3,038 3,322 4,260 ence with Pajaro puted for this stre	* * * * River am	* * * * *	49.5 51.7 52.7 56.7 56.7	* * * *	* * * * *	* * * *	* * * *
Ţ	FEDERAL EI	MERGENCY MA		AGENCY		EI			
ABLE 24			TY, CALIF	ORNIA		FLOODING S	OURCE: THOM		EEK

LOCA	TION		FLOODWAY		1% ANNUAL CH	IANCE FLOOD W (FEET NA	ATER SURFACE	ELEVATION
CROSS SECTION	DISTANCE1	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
A <sup>2</sup> B <sup>2</sup> C <sup>2</sup> D <sup>2</sup> E <sup>2</sup> F <sup>2</sup> G <sup>2</sup> H <sup>2</sup> I <sup>2</sup>	1,190 2,610 3,978 4,121 5,540 7,208 7,332 8,460 11,100 11,100	* * * * * *	* * * * * * * * *	* * * * * * * * *	48.3 48.3 52.8 53.8 58.8 73.5 73.5 83.6 115.7	* * * * * * * * *	* * * * * * * *	* * * * * * * * * *
FEDERAL			AGENCY		FL	OODWAY	DATA	
	RUZ COUN	TY, CALIF	ORNIA		FLOODING	SOURCE: THO		EK

ELEVATIO	ATER SURFACE	ANCE FLOOD W FEET NA	1% ANNUAL CH		FLOODWAY		ION	LOCA
INCREAS	WITH FLOODWAY	WITHOUT FLOODWAY <sup>3</sup>	REGULATORY	MEAN VELOCITY (FEET/SEC)	SECTION AREA (SQ. FEET)	WIDTH (FEET)	DISTANCE <sup>1</sup>	CROSS SECTION
0.0		44.5	10.0		0 705	$aaa^2$	100	
0.0	11.5	11.5	13.0	1.4	2,725	626 <sup>-</sup>	400	A
0.0	11.7	11.7	13.6	1.0	3,813	/91 <sup>-</sup>	1,680	В
0.0	11.8	11.8	14.0	0.9	4,230	1,050-	2,880	C
0.1	11.9	11.8	14.4	0.9	4,076	847	3,920	D
0.1	12.0	11.9	14.8	0.6	662	1,30 <u>6</u>	5,120	E
0.1	12.1	12.0	15.2	0.9	4,147	800 <sup>2</sup>	6,220	F
0.1	12.1	12.0	15.5	1.4	2,862	800 <sup>2</sup>	6,375	G
0.6	12.6	12.0	15.6	1.7	2,307	1,150 <sup>2</sup>	7,680	Н
0.6	12.6	12.0	15.7	0.7	5,869	950 <sup>2</sup>	7,980	I
0.7	12.7	12.0	15.8	0.8	4,582	942 <sup>2</sup>	9,090	J
0.7	12.8	12.1	15.9	0.9	4,343	959 <sup>2</sup>	10,290	K
0.8	12.9	12.1	16.0	0.8	4,833	950 <sup>2</sup>	11,770	L
0.8	13.0	12.2	16.2	0.9	4,268	900 <sup>2</sup>	12,940	М
0.8	13.1	12.3	16.3	0.9	4,289	900 <sup>2</sup>	14.220	Ν
0.8	13.1	12.3	16.6	0.9	4,103	900 <sup>2</sup>	14.940	0
0.1	14.2	14.1	16.7	0.9	4,406	$750^{2}$	15,180	P
0.2	14.3	14.1	17.0	1.8	715	$100^{2}$	17.915	Q
0.0	14.9	14.9	17.0	16	796	$100^{2}$	18 185	R
0.5	15.4	14.9	17.4	1.4	922	100	22,420	S
0.7	15.6	14.9	17.5	1.9	215	30	23,830	Ť
0.7	15.6	14.9	18.5	19	218	30	24,065	U
0.7	15.8	15.0	22.3	1.0	242	30	24,000	V

<sup>1</sup>Feet above confluence with Pajaro River

TABLE

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<sup>2</sup>Width of map may be greater due to combined floodway with Pajaro River

<sup>3</sup>Elevation computed without consideration of influence from Pajaro River

#### FEDERAL EMERGENCY MANAGEMENT AGENCY

## SANTA CRUZ COUNTY, CALIFORNIA

#### AND INCORPORATED AREAS

## **FLOODWAY DATA**

#### FLOODING SOURCE: WATSONVILLE SLOUGH

LOCATION FLOODWAY			1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATION (FEET NAVD88)					
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
W X Y Z AA AB AC AD AE AF AG AH AI AJ AK AL	25,340 26,190 26,310 27,150 27,960 28,080 28,655 29,519 29,576 30,379 31,648 32,647 33,022 33,484 34,246 35,531	30 30 30 49 50 365 350 351 359 314 271 60 33 28 22	274 159 231 194 329 3,502 2,863 2,854 3,056 5,174 3,265 637 130 127 34	1.5 2.6 1.8 2.1 1.2 1.0 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	23.2 24.0 24.1 25.7 25.7 25.7 25.8 25.8 25.8 25.8 26.1 26.1 26.1 26.3 39.7 59.1	$15.1^{2}$ $15.3^{2}$ $16.9^{2}$ $17.0^{2}$ $17.0^{2}$ $16.9^{2}$ $16.9^{2}$ $16.9^{2}$ $16.9^{2}$ $26.4$ $26.4$ $26.5$ $39.7$ $59.1$	$\begin{array}{c} 15.9\\ 16.1\\ 17.0\\ 17.4\\ 17.6\\ 16.8\\ 17.7\\ 17.7\\ 17.7\\ 17.7\\ 26.8\\ 26.8\\ 26.8\\ 26.8\\ 26.9\\ 40.4\\ 59.2 \end{array}$	0.8 0.8 0.1 0.4 0.6 0.2 0.8 0.8 0.8 0.8 0.8 0.8 0.4 0.4 0.4 0.4 0.4 0.7 0.1
<sup>2</sup> Elevation compu	ence with Pajaro Ri	ver eration of influ	ence from Pajaro	) River				
FEDERAL I					FL	OODWAY	DATA	
	ND INCORPORA			FLOODING SOURCE: WATSONVILLE SLOUGH				

1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATION (FEET NAVD88)				FLOODWAY			LOCATION	
INCREASE	WITH FLOODWAY	WITHOUT FLOODWAY	REGULATORY	MEAN VELOCITY (FEET/SEC)	SECTION AREA (SQ. FEET)	WIDTH (FEET)	DISTANCE <sup>1</sup>	CROSS SECTION
0.0	$acc a^2$	$aca a^2$	005.4	477	004	4.4	005	•
0.0	262.8	262.8	265.1	17.7	664	41	905	A
0.0	268.0	268.0	268.0	6.6	1,778	181	1,055	В
0.0	268.5	268.5	268.5	10.6	1,103	117	1,745	
0.0	270.8	270.8	270.8	7.5	1,560	120	2,435	D
0.0	271.3	271.3	2/1.3	8.0	1,467	118	2,600	E
0.0	273.7	2/3./	2/3./	13.2	636	66	3,250	F
0.0	281.0	281.0	281.0	13.6	619	67	4,200	G
0.0	286.4	286.4	286.4	8.4	1,000	88	4,845	Н
0.0	287.4	287.4	287.4	9.5	888	98	5,000	I
0.0	292.4	292.4	292.4	11.2	750	97	5,810	J
0.0	300.1	300.1	300.1	6.0	1,406	126	7,065	K
0.0	301.2	301.2	301.2	4.8	1,761	163	7,245	L
0.0	301.6	301.6	301.6	7.8	1,078	126	7,780	М
0.0	304.0	304.0	304.0	11.3	630	74	8,500	Ν
0.0	308.7	308.7	308.7	9.5	882	104	8,990	0
0.0	317.7	317.7	317.7	11.4	734	78	10,570	Р
0.0	322.3	322.3	322.3	9.3	899	86	11,150	Q
0.0	324.5	324.5	324.5	10.3	811	70	11,730	R
0.0	325.7	325.7	325.7	12.3	636	64	12,080	S
0.0	331.4	331.4	331.4	14.9	528	64	12,790	Т
0.0	335.8	335.8	335.8	12.8	612	89	13,140	U
0.0	338.9	338.9	338.9	11.0	714	83	13,260	V
0.0	348.5	348.5	348.5	10.6	741	92	14,830	Ŵ

<sup>1</sup>Feet above confluence with San Lorenzo River

TABLE 24

<sup>2</sup>Elevation computed without consideration of backwater from San Lorenzo River

### FEDERAL EMERGENCY MANAGEMENT AGENCY

SANTA CRUZ COUNTY, CALIFORNIA

## FLOODWAY DATA

AND INCORPORATED AREAS

FLOODING SOURCE: ZAYANTE CREEK

LOCATION FLOOD		FLOODWAY		1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATIO (FEET NAVD88)				
CROSS SECTION	DISTANCE <sup>1</sup>	WIDTH (FEET)	SECTION AREA (SQ. FEET)	MEAN VELOCITY (FEET/SEC)	REGULATORY	WITHOUT FLOODWAY	WITH FLOODWAY	INCREASE
X	40.050	0.0	745	40.5	050.4	050.4	250.4	0.0
X	16,250	88	745	10.5	356.4	356.4	356.4	0.0
Y 7	16,530	65	640	9.5	358.5	358.5	358.5	0.0
Z	16,840	53	390	15.5	359.8	359.8	359.8	0.0
AA	17,500	//	486	12.5	3/1.8	371.8	371.8	0.0
AB	18,040	76	449	13.5	378.1	378.1	378.1	0.0
AC	18,580	86	558	10.9	384.7	384.7	384.7	0.0
AD	18,700	117	1,174	5.2	392.0	392.0	392.0	0.0
AE	18,930	110	954	6.3	392.2	392.2	392.2	0.0
AF	19,190	40	357	17.0	398.0	398.0	398.0	0.0
AG	19,840	89	800	7.6	405.2	405.2	405.2	0.0
AH	20,240	69	438	13.8	407.6	407.6	407.6	0.0
AI	20,650	88	739	8.2	413.0	413.0	413.0	0.0
AJ	20,770	70	6,621	9.7	413.3	413.3	413.3	0.0
AK	21,170	50	382	15.8	415.9	415.9	415.9	0.0
AL	21,560	62	433	14.0	423.0	423.0	423.0	0.0
AM	22,030	62	445	13.6	429.4	429.4	429.4	0.0
AN	22,490	56	475	12.7	434.6	434.6	434.6	0.0
AO	23,100	56	470	12.9	440.0	440.0	440.0	0.0
AP	23,700	27	313	19.3	450.6	450.6	450.6	0.0
AQ	24,230	32	486	12.4	461.5	461.5	461.5	0.0
AR	24,750	52	653	9.3	465.4	465.4	465.4	0.0
AS	25.930	65	643	9.4	470.1	470.1	470.1	0.0
AT	26,050	64	614	9.9	470.6	470.6	470.6	0.0
Feet above conflu	ence with San Lore	nzo River						
FEDERAL I	EMERGENCY MA	NAGEMENT	AGENCY		FI	OODWAY	DATA	
SANTA C	RUZ COUN	TY, CALIF	ORNIA					

AND INCORPORATED AREAS

## Table 25: Flood Hazard and Non-Encroachment Data for Selected Streams[Not Applicable to this Flood Risk Project]

#### 6.4 Coastal Flood Hazard Mapping

Flood insurance zones and BFEs including the wave effects were identified on each transect based on the results from the onshore wave hazard analyses. Between transects, elevations were interpolated using topographic maps, land-use and land-cover data, and knowledge of coastal flood processes to determine the aerial extent of flooding. Sources for topographic data are shown in Table 23.

Zone VE is subdivided into elevation zones and BFEs are provided on the FIRM.

The limit of Zone VE shown on the FIRM is defined as the farthest inland extent of any of these criteria (determined for the 1% annual chance flood condition):

- The *primary frontal dune zone* is defined in 44 CFR Section 59.1 of the NFIP regulations. The primary frontal dune represents a continuous or nearly continuous mound or ridge of sand with relatively steep seaward and landward slopes that occur immediately landward and adjacent to the beach. The primary frontal dune zone is subject to erosion and overtopping from high tides and waves during major coastal storms. The inland limit of the primary frontal dune zone occurs at the point where there is a distinct change from a relatively steep slope to a relatively mild slope.
- The *wave runup zone* occurs where the (eroded) ground profile is 3.0 feet or more below the 2-percent wave runup elevation.
- The *wave overtopping splash zone* is the area landward of the crest of an overtopped barrier, in cases where the potential 2-percent wave runup exceeds the barrier crest elevation by 3.0 feet or more.
- The *breaking wave height zone* occurs where 3-foot or greater wave heights could occur (this is the area where the wave crest profile is 2.1 feet or more above the total stillwater elevation).
- The *high-velocity flow zone* is landward of the overtopping splash zone (or area on a sloping beach or other shore type), where the product of depth of flow times the flow velocity squared (hv<sup>2</sup>) is greater than or equal to 200 ft<sup>3</sup>/sec<sup>2</sup>. This zone may only be used on the Pacific Coast.

The SFHA boundary indicates the limit of SFHAs shown on the FIRM as either "V" zones or "A" zones.

Table 26 indicates the coastal analyses used for floodplain mapping and the criteria used to determine the inland limit of the open-coast Zone VE and the SFHA boundary at each transect.

		Wave Runup Analysis	Wave Height Analysis		
Coastal Transect	Primary Frontal Dune (PFD) Identified	Zone Designation and BFE (ft NAVD 88)	Zone Designation and BFE (ft NAVD 88)	Zone VE Limit	SFHA Boundary
1		VE 20	N/A	Runup	Runup
2		VE 38	N/A	Overtopping	Overtopping
3		VE 22	N/A	Overtopping	Overtopping
4		VE 21	N/A	Runup	Runup
5		VE 17	N/A	Runup	Runup
6		VE 18	N/A	Runup	Runup
7		VE 20	N/A	Runup	Runup
8		VE 23	N/A	Runup	Runup
9		VE 21	N/A	Overtopping	Overtopping
10		VE 17	N/A	Runup	Runup
11		VE 19	N/A	Runup	Runup
12		VE 19	N/A	Overtopping	Overtopping
13		VE 21	N/A	Overtopping	Overtopping
14		VE 26	N/A	Runup	Runup
15		VE 19	N/A	Runup	Runup
16		VE 27	N/A	Runup	Runup
17	~	VE 17	N/A	PFD	PFD
18		VE 32	N/A	Runup	Runup
19		VE 24	N/A	Runup	Runup
20		VE 32	N/A	Runup	Runup
21		VE 38	N/A	Overtopping	Overtopping
22		VE 31	N/A	Runup	Runup
23		VE 27	N/A	Runup	Runup
24		VE 34	N/A	Runup	Runup
25		VE 33	N/A	Runup	Runup
26		VE 24	N/A	Runup	Runup
27		VE 29	N/A	Runup	Runup
28		VE 32	N/A	Runup	Runup
29		VE 13	N/A	Runup	Runup
30		VE 18	N/A	Overtopping	Overtopping

Table 26: Summar	of Coastal Transect Mapping Co	onsiderations
	· · · · · · · · · · · · · · · · · · ·	

		Wave Runup Analysis	Wave Height Analysis		
Coastal Transect	Primary Frontal Dune (PFD) Identified	Zone Designation and BFE (ft NAVD 88)	Zone Designation and BFE (ft NAVD 88)	Zone VE Limit	SFHA Boundary
31		VE 18	N/A	Overtopping	Overtopping
32		VE 19	N/A	Runup	Runup
33		VE 19	N/A	Overtopping	Overtopping
34		VE 20	N/A	Runup	Runup
35		VE 17	N/A	Runup	Runup
36		VE 31	N/A	Runup	Runup
37		VE 19	N/A	Runup	Runup
38		VE 18	N/A	Overtopping	Overtopping
39		VE 20	N/A	Runup	Runup
40		VE 20	N/A	Runup	Runup
41		VE 31	N/A	Runup	Runup
42		VE 42	N/A	Overtopping	Overtopping
43		VE 23	N/A	Runup	Runup
44		VE 35	N/A	Runup	Runup
45		VE 29	N/A	Runup	Runup
46		VE 16	N/A	Runup	Runup
47		VE 18	N/A	Overtopping	Overtopping
48		VE 20	N/A	Overtopping	Overtopping
49		VE 24	N/A	Runup	Runup
50		VE 22	N/A	Runup	Runup
51		VE 20	N/A	Runup	Runup
52		VE 23	N/A	Runup	Runup
53		VE 19	N/A	Runup	Runup
54		VE 25	N/A	Overtopping	Overtopping
55		VE 23	N/A	Runup	Runup
56		VE 26	N/A	Overtopping	Overtopping
57		VE 21	N/A	Overtopping	Overtopping
58		VE 21	N/A	Runup	Runup
59		VE 22	N/A	Runup	Runup
60		VE 20	N/A	Runup	Runup
61		VE 21	N/A	Runup	Runup

		Wave Runup Analysis	Wave Height Analysis		
Coastal Transect	Primary Frontal Dune (PFD) Identified	Zone Designation and BFE (ft NAVD 88)	Zone Designation and BFE (ft NAVD 88)	Zone VE Limit	SFHA Boundary
62		VE 23	N/A	Runup	Runup
63		VE 18	N/A	Runup	Runup
64		VE 21	N/A	Runup	Runup
65		VE 16	N/A	Runup	Runup
66		VE 20	N/A	Runup	Runup
67		VE 20	N/A	Runup	Runup
68		VE 19	N/A	Runup	Runup
69	~	VE 18	N/A	PFD	PFD
70	~	VE 19	N/A	PFD	PFD
71	~	VE 22	N/A	PFD	PFD
72	~	VE 21	N/A	Runup	PFD

#### 6.5 **FIRM Revisions**

This FIS Report and the FIRM are based on the most up-to-date information available to FEMA at the time of its publication; however, flood hazard conditions change over time. Communities or private parties may request flood map revisions at any time. Certain types of requests require submission of supporting data. FEMA may also initiate a revision. Revisions may take several forms, including Letters of Map Amendment (LOMAs), Letters of Map Revision Based on Fill (LOMR-Fs), Letters of Map Revision (LOMRs) (referred to collectively as Letters of Map Change (LOMCs)), Physical Map Revisions (PMRs), and FEMA-contracted restudies. These types of revisions are further described below. Some of these types of revisions, it is advisable to contact the community repository of flood-hazard data (shown in Table 31, "Map Repositories").

#### 6.5.1 Letters of Map Amendment

A LOMA is an official revision by letter to an effective NFIP map. A LOMA results from an administrative process that involves the review of scientific or technical data submitted by the owner or lessee of property who believes the property has incorrectly been included in a designated SFHA. A LOMA amends the currently effective FEMA map and establishes that a specific property is not located in a SFHA. A LOMA cannot be issued for properties located on the PFD (primary frontal dune).

To obtain an application for a LOMA, visit www.fema.gov/floodplain-management/letter-mapamendment-loma and download the form "MT-1 Application Forms and Instructions for Conditional and Final Letters of Map Amendment and Letters of Map Revision Based on Fill". Visit the "Flood Map-Related Fees" section to determine the cost, if any, of applying for a LOMA.

FEMA offers a tutorial on how to apply for a LOMA. The LOMA Tutorial Series can be accessed at www.fema.gov/online-tutorials.

For more information about how to apply for a LOMA, call the FEMA Map Information eXchange; toll free, at 1-877-FEMA MAP (1-877-336-2627).

#### 6.5.2 Letters of Map Revision Based on Fill

A LOMR-F is an official revision by letter to an effective NFIP map. A LOMR-F states FEMA's determination concerning whether a structure or parcel has been elevated on fill above the base flood elevation and is, therefore, excluded from the SFHA.

Information about obtaining an application for a LOMR-F can be obtained in the same manner as that for a LOMA, by visiting www.fema.gov/floodplain-management/letter-map-amendment-loma for the "MT-1 Application Forms and Instructions for Conditional and Final Letters of Map Amendment and Letters of Map Revision Based on Fill" or by calling the FEMA Map Information eXchange, toll free, at 1-877-FEMA MAP (1-877-336-2627). Fees for applying for a LOMR-F, if any, are listed in the "Flood Map-Related Fees" section.

A tutorial for LOMR-F is available at www.fema.gov/online-tutorials.

#### 6.5.3 Letters of Map Revision

A LOMR is an official revision to the currently effective FEMA map. It is used to change flood zones, floodplain and floodway delineations, flood elevations and planimetric features. All requests for LOMRs should be made to FEMA through the chief executive officer of the community, since it is the community that must adopt any changes and revisions to the map. If the request for a LOMR is not submitted through the chief executive officer of the community, evidence must be submitted that the community has been notified of the request.

To obtain an application for a LOMR, visit www.fema.gov/national-flood-insurance-programflood-hazard-mapping/mt-2-application-forms-and-instruction and download the form "MT-2 Application Forms and Instructions for Conditional Letters of Map Revision and Letters of Map Revision". Visit the "Flood Map-Related Fees" section to determine the cost of applying for a LOMR. For more information about how to apply for a LOMR, call the FEMA Map Information eXchange; toll free, at 1-877-FEMA MAP (1-877-336-2627) to speak to a Map Specialist.

Previously issued mappable LOMCs (including LOMRs) that have been incorporated into the Santa Cruz County FIRM are listed in Table 27.

#### Table 27: Incorporated Letters of Map Change

#### [Not Applicable to this Flood Risk Project]

#### 6.5.4 Physical Map Revisions

Physical Map Revisions (PMRs) are an official republication of a community's NFIP map to effect changes to base flood elevations, floodplain boundary delineations, regulatory floodways and planimetric features. These changes typically occur as a result of structural works or improvements, annexations resulting in additional flood hazard areas or correction to base flood elevations or SFHAs.

The community's chief executive officer must submit scientific and technical data to FEMA to support the request for a PMR. The data will be analyzed and the map will be revised if warranted. The community is provided with copies of the revised information and is afforded a review period. When the base flood elevations are changed, a 90-day appeal period is provided. A 6-month adoption period for formal approval of the revised map(s) is also provided.

For more information about the PMR process, please visit www.fema.gov and visit the "Flood Map Revision Processes" section.

#### 6.5.5 Contracted Restudies

The NFIP provides for a periodic review and restudy of flood hazards within a given community. FEMA accomplishes this through a national watershed-based mapping needs assessment strategy, known as the Coordinated Needs Management Strategy (CNMS). The CNMS is used by FEMA to assign priorities and allocate funding for new flood hazard analyses used to update the FIS Report and FIRM. The goal of CNMS is to define the validity of the engineering study data within a mapped inventory. The CNMS is used to track the assessment process, document engineering gaps and their resolution, and aid in prioritization for using flood risk as a key factor for areas identified for flood map updates. Visit www.fema.gov to learn more about the CNMS or contact the FEMA Regional Office listed in Section 8 of this FIS Report.

#### 6.5.6 Community Map History

The current FIRM presents flooding information for the entire geographic area of Santa Cruz County. Previously, separate FIRMs, Flood Hazard Boundary Maps (FHBMs) and/or Flood Boundary and Floodway Maps (FBFMs) may have been prepared for the incorporated communities and the unincorporated areas in the county that had identified SFHAs. Current and historical data relating to the maps prepared for the project area are presented in Table 28, "Community Map History." A description of each of the column headings and the source of the date is also listed below.

- *Community Name* includes communities falling within the geographic area shown on the FIRM, including those that fall on the boundary line, nonparticipating communities, and communities with maps that have been rescinded. Communities with No Special Flood Hazards are indicated by a footnote. If all maps (FHBM, FBFM, and FIRM) were rescinded for a community, it is not listed in this table unless SFHAs have been identified in this community.
- *Initial Identification Date (First NFIP Map Published)* is the date of the first NFIP map that identified flood hazards in the community. If the FHBM has been converted to a FIRM, the initial FHBM date is shown. If the community has never been mapped, the upcoming effective date or "pending" (for Preliminary FIS Reports) is shown. If the community is listed in Table 28 but not identified on the map, the community is treated as if it were unmapped.

- *Initial FHBM Effective Date* is the effective date of the first Flood Hazard Boundary Map (FHBM). This date may be the same date as the Initial NFIP Map Date.
- *FHBM Revision Date(s)* is the date(s) that the FHBM was revised, if applicable.
- *Initial FIRM Effective Date* is the date of the first effective FIRM for the community. This is the first effective date that is shown on the FIRM panel.
- *FIRM Revision Date(s)* is the date(s) the FIRM was revised, if applicable. This is the revised date that is shown on the FIRM panel, if applicable. As countywide studies are completed or revised, each community listed should have its FIRM dates updated accordingly to reflect the date of the countywide study. Once the FIRMs exist in countywide format, as Physical Map Revisions (PMR) of FIRM panels within the county are completed, the FIRM Revision Dates in the table for each community affected by the PMR are updated with the date of the PMR, even if the PMR did not revise all the panels within that community.

The initial effective date for the Santa Cruz County FIRMs in countywide format was 03/02/2006.

Community Name	Initial Identification Date	Initial FHBM Effective Date	FHBM Revision Date(s)	Initial FIRM Effective Date	FIRM Revision Date(s)
Capitola, City of	05/17/1974	05/17/1974	03/19/1976	08/15/1984	09/29/2017 05/16/2012 03/02/2006
Santa Cruz, City of	03/08/1974	03/08/1974	04/23/1976	02/15/1985	09/29/2017 05/16/2012 03/02/2006
Santa Cruz County, Unincorporated Areas	08/16/1974	08/16/1974	05/29/1979	04/15/1986	09/29/2017 05/16/2012 03/02/2006
Scotts Valley, City of	05/31/1974	05/31/1974	11/07/1975	10/18/1983	05/16/2012 03/02/2006
Watsonville, City of	03/22/1974	03/22/1974	11/21/1975	06/15/1984	05/16/2012 03/02/2006

Table 28: Community Map History

#### SECTION 7.0 – CONTRACTED STUDIES AND COMMUNITY COORDINATION

#### 7.1 Contracted Studies

Table 29 provides a summary of the contracted studies, by flooding source, that are included in this FIS Report.

Flooding Source	FIS Report Dated	Contractor	Number	Work Completed Date	Affected Communities
Aptos Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Arana Gulch	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Baldwin Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Bean Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas; Scotts Valley, City of
Bear Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Boulder Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Branciforte Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz, City of; Santa Cruz County, Unincorporated Areas
Browns Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Carbonera Creek	04/18/1983	Brown and Caldwell	H-4723	November 1982	Scotts Valley, City of
College Lake	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Corralitos Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas

## Table 29: Summary of Contracted Studies Included in this FIS Report

Flooding Source	FIS Report Dated	Contractor	Number	Work Completed Date	Affected Communities
Coward Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Drew Lake	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Gallighan Slough	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Hanson Slough	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Hare Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Harkins Slough	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Hopkins Gulch	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Kelly Lake	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Kings Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Laguna Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Lake Tynan	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Flooding Source	FIS Report Dated	Contractor	Number	Work Completed Date	Affected Communities
--------------------------	---------------------	-----------------------	---	---------------------------	--
Loch Lomond Reservoir	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Lompico Creek	05/16/2012	BakerAECOM, LLC	HSFEHQ-09- D-0368, Task Order HSFE09-09- J-0001	July 2011	Santa Cruz County, Unincorporated Areas
Love Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Majors Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Mill Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Molino Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Moore Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Moran Lake	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Newell Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Nobel Creek	06/03/1986	Brown and Caldwell	H-4723	May 1983	Capitola, City of
Old Dairy Gulch	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas

Flooding Source	FIS Report Dated	Contractor	Number	Work Completed Date	Affected Communities
Pacific Ocean	09/29/2017	BakerAECOM	HSFEHQ-09- D-0368, Task Order HSFE09-10- J-0002	August 2013	Capitola, City of; Santa Cruz, City of; Santa Cruz County Unincorporated Areas; Watsonville, City of
Pajaro River	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas; Watsonville, City of
Pinto Lake	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas; Watsonville, City of
Rodeo Creek Gulch	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Rose Reservoir	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Salsipuedes Creek	05/16/2012	Philip Williams and Associates, Ltd.	FEMA Task Order No. 5	May 2009	Santa Cruz County, Unincorporated Areas; Watsonville, City of
San Lorenzo River	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz, City of; Santa Cruz County, Unincorporated Areas
San Vicente Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Schwans Lagoon	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas

Flooding Source	FIS Report Dated	Contractor	Number	Work Completed Date	Affected Communities
Scott Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Soquel Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Capitola, City of; Santa Cruz County, Unincorporated Areas
Struve Slough	05/16/2012	Philip Williams and Associates, Ltd.	FEMA Task Order No. 5	May 2009	Santa Cruz County, Unincorporated Areas; Watsonville, City of
Thomasello Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Thompson Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Two Bar Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Waddell Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Watsonville Slough	05/16/2012	Philip Williams and Associates, Ltd.	FEMA Task Order No. 5	May 2009	Santa Cruz County, Unincorporated Areas; Watsonville, City of
West Branch Struve Slough	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas
Wilder Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas

Flooding Source	FIS Report Dated	Contractor	Number	Work Completed Date	Affected Communities
Zayante Creek	04/15/1986	Brown and Caldwell	H-4723	April 1983	Santa Cruz County, Unincorporated Areas

### 7.2 Community Meetings

The dates of the community meetings held for this Flood Risk Project and any previous Flood Risk Projects are shown in Table 30. These meetings may have previously been referred to by a variety of names (Community Coordination Officer (CCO), Scoping, Discovery, etc.), but all meetings represent opportunities for FEMA, community officials, study contractors, and other invited guests to discuss the planning for and results of the project.

# Table 30: Community Meetings

Community	FIS Report Dated	Date of Meeting	Meeting Type	Attended By
Capitola, City of	00/20/2017	11/13/2014	FRR	FEMA, this community and the study contractor (BakerAECOM)
	09/29/2017	10/15/2015	ссо	FEMA, this community and the study contractor (BakerAECOM)
Santa Cruz, City of	00/20/2017	11/13/2014	FRR	FEMA, this community and the study contractor (BakerAECOM)
	09/29/2017	10/15/2015	ссо	FEMA, this community and the study contractor (BakerAECOM)
Santa Cruz County	09/29/2017	11/13/2014	FRR	FEMA, this community and the study contractor (BakerAECOM)
(Unincorporated Areas)		10/15/2015	ссо	FEMA, this community and the study contractor (BakerAECOM)
Seatta Vallay, City of	*	04/1978	Initial CCO	FEMA, this community and the study contractor
Scotts valley, City of		04/22/1992	Final CCO	FEMA, this community and the study contractor
Watsonville, City of	05/16/2012	02/10/2010	Initial CCO	FEMA, this community and the study contractor (BakerAECOM)
		02/15/2011	Final CCO	FEMA, this community and the study contractor (BakerAECOM)

\*Data not available

### **SECTION 8.0 – ADDITIONAL INFORMATION**

Information concerning the pertinent data used in the preparation of this FIS Report can be obtained by submitting an order with any required payment to the FEMA Engineering Library. For more information on this process, see www.fema.gov.

Table 31 is a list of the locations where FIRMs for Santa Cruz County can be viewed. Please note that the maps at these locations are for reference only and are not for distribution. Also, please note that only the maps for the community listed in the table are available at that particular repository. A user may need to visit another repository to view maps from an adjacent community.

Community	Address	City	State	Zip Code
Capitola, City of	City Hall 420 Capitola Ave	Capitola	CA	95010
Santa Cruz, City of	City Hall Planning Department: Permits, Building, Zoning 809 Center Street Room 206	Santa Cruz	CA	95060
Santa Cruz County, Unincorporated Areas	County of Santa Cruz Planning Department 701 Ocean Street 4 <sup>th</sup> Floor	Santa Cruz	CA	95060
Scotts Valley, City of	Planning Department 1 Civic Center Drive	Scotts Valley	CA	95066
Watsonville, City of	Community Development Department 250 Main Street	Watsonville	CA	95076

Table 31: Map Repositories

The National Flood Hazard Layer (NFHL) dataset is a compilation of effective FIRM databases and LOMCs. Together they create a GIS data layer for a State or Territory. The NFHL is updated as studies become effective and extracts are made available to the public monthly. NFHL data can be viewed or ordered from the website shown in Table 32.

Table 32 contains useful contact information regarding the FIS Report, the FIRM, and other relevant flood hazard and GIS data. In addition, information about the state NFIP Coordinator and GIS Coordinator is shown in this table. At the request of FEMA, each Governor has designated an agency of State or territorial government to coordinate that State's or territory's NFIP activities. These agencies often assist communities in developing and adopting necessary floodplain management measures. State GIS Coordinators are knowledgeable about the availability and location of state and local GIS data in their state.

	FEMA and the NFIP			
FEMA and FEMA Engineering Library website	www.fema.gov/national-flood-insurance-program-flood- hazard-mapping/engineering-library			
NFIP website	www.fema.gov/national-flood-insurance-program			
NFHL Dataset	msc.fema.gov			
FEMA Region IX	FEMA Region IX 1111 Broadway, Suite 1200, Oakland, CA 94607 (510) 627-7029			
Other Federal Agencies				
USGS website	www.usgs.gov			
Hydraulic Engineering Center website	www.hec.usace.army.mil			
	State Agencies and Organizations			
State NFIP Coordinator	Ricardo Pineda, PE, CFM California Dept. of Water Resources 1416 9 <sup>th</sup> Street, Room 1601 Sacramento, CA 95814 916-574-0611 rpineda@water.ca.gov			
State GIS Coordinator	David Harris Agency Information Officer California Natural Resources Agency 1416 Ninth Street, Room 1311 Sacramento, CA 95814 916-445-5088 david.harris@resources.ca.gov			

#### **Table 32: Additional Information**

# SECTION 9.0 – BIBLIOGRAPHY AND REFERENCES

Table 33 includes sources used in the preparation of and cited in this FIS Report as well as additional studies that have been conducted in the study area.

Citation in this FIS	Publisher/ Issuer	<i>Publication Title,</i> "Article," Volume, Number, etc.	Author/Editor	Place of Publication	Publication Date/ Date of Issuance	Link
AECOM 2008	AECOM Watershed Concepts	Watershed Information System (WISE) version 4.1		Roanoke, VA	2008	
Ben B. White & Assoc. 1965	Ben B. White & Associates, Inc.	City of Capitola Topographic Maps, Scale 1:600, Contour Interval 2 feet			October 25, 1965	
Briggs 1982	Department of Earth Sciences, University of California at Santa Cruz	Impact of the January 3- 4, 1982, Floods in Santa Cruz County, California	Gary B. Briggs		1982	
City of Santa Cruz 1974	City of Santa Cruz	Topographic Maps, Scale 1:1,200, Contour Interval 4 feet	Murray- McCormick Aerial Surveys, Inc.		October 15, 1974	
Commerce 2010	U.S. Department of Commerce, National Climatic Data Center,	Storm Events [online]			May 18, 2010	http://www4.ncdc.noaa.gov
DOI 1977	U.S. Department of the Interior, Geological Survey	Water Resources Investigations Report 77-21, Magnitude and Frequency of Floods in California			June 1977	
Otto Water Engineers, Inc. 1984	Federal Emergency Management Agency	Northern California Coastal Flood Studies	Otto Water Engineers, Inc.		August 1984	

Citation in this FIS	Publisher/ Issuer	<i>Publication Title,</i> "Article," Volume, Number, etc.	Author/Editor	Place of Publication	Publication Date/ Date of Issuance	Link
Philip Williams & Assoc. 2009	Philip Williams & Associates, Ltd.	Hydraulic Analysis for Santa Cruz County, CA, FEMA Task Order No. 5			May 2009	
Santa Cruz County 1965	Santa Cruz County	San Lorenzo River Basin Topographic Maps, Scale 1:4,800, Contour Interval 20 feet			1965	
Santa Cruz County, Office of Watershed 1979	Santa Cruz County, Office of Watershed Management	San Lorenzo River Watershed Management Plan, Draft			May 1979	
Spink Corp. 1978	Spink Corporation	Aerial Photography, Scale 1:4,800, Contour Interval 4 feet		Sacramento, CA	1978	
State of California DWR 1975	State of California, The Resources Agency, Department of Water Resources	Bulletin No. 195, Rainfall Analysis for Drainage Design Volume III – Intensity-Duration- Frequency Curves			October 1975	
USACE 2008	U.S. Department of the Army, Corps of Engineers, Hydrologic Engineering Center	HEC- RAS (River Analysis System) version 4.0		Davis, CA	March 2008	

Citation in this FIS	Publisher/ Issuer	<i>Publication Title,</i> "Article," Volume, Number, etc.	Author/Editor	Place of Publication	Publication Date/ Date of Issuance	Link
USACE 2004	U.S. Department of the Army, Corps of Engineers, Hydrologic Engineering Center	HEC- RAS (River Analysis System) version 3.1.2		Davis, CA	June 2004	
USACE 1979	U.S. Department of the Army, Corps of Engineers, San Francisco District	San Lorenzo River Reconnaissance Study			December 1979	
USACE 1979	U.S. Department of the Army, Corps of Engineers, Waterway Experiment Station	A Numerical Model for Tsunami Inundation, Technical Report HL-79- 2	J.R. Houston and A.W. Garcia		February 1979	
USACE 1976	U.S. Department of the Army, Corps of Engineers	Floodplain Information, Corralitos Creek, Santa Cruz County, California		San Francisco, CA	June 1976	
USACE June 1976	U.S. Department of the Army, Corps of Engineers	Floodplain Information, Soquel Creek, Santa Cruz County, California		San Francisco, CA	June 1976	
USACE 1973 (a.)	U.S. Department of the Army, Corps of Engineers	Floodplain Information, Aptos, Trout, and Valencia Creek, City of Aptos, California State		San Francisco, CA	July 1973	
USACE 1973 (b.)	U.S. Department of the Army, Corps of Engineers	Floodplain Information, San Lorenzo River, Santa Cruz County, California		San Francisco, CA	July 1973	

Citation in this FIS	Publisher/ Issuer	<i>Publication Title,</i> "Article," Volume, Number, etc.	Author/Editor	Place of Publication	Publication Date/ Date of Issuance	Link
USACE January 1973	U.S. Department of the Army, Corps of Engineers, Hydrologic Engineering Center	HEC-1 Flood Hydrograph Package Users Manual		Davis, CA	January 1973	
USACE 1971	U.S. Department of the Army, Corps of Engineers	Pajaro River Topographic Maps, Scale 1:1,200, Contour Interval 2 feet			1971	
USACE 1968	U.S. Department of the Army, Corps of Engineers, Hydrologic Engineering Center	Computer Program 723- X6-L2010, HEC-1 Flood Hydrograph Package		Davis, CA	October 1968 with updates	
USACE 1965	U.S. Department of the Army, Corps of Engineers	Survey Report – Flood Control and Allied Purposes, Soquel Creek, Santa Cruz County, California		San Francisco, CA	November 1963, revised May 1965	
USACE 1963	U.S. Department of the Army, Corps of Engineers	Interim Report for Flood Control, Pajaro River Basin, California		San Francisco, CA	June 1963	
USACE 1956	U.S. Department of the Army, Corps of Engineers	Floods of December 1955 and January 1956 in Northern California Coastal Streams		San Francisco, CA	June 1956	
USACE General Design Memoran- dum	U.S. Department of the Army, Corps of Engineers	General Design Memorandum – San Lorenzo River Flood Control Project				

Citation in this FIS	Publisher/ Issuer	<i>Publication Title,</i> "Article," Volume, Number, etc.	Author/Editor	Place of Publication	Publication Date/ Date of Issuance	Link
USGS 2009-2011	U.S. Geological Survey	LiDAR data			2009-2011	
USWRC 1977	U.S. Water Resources Council	Bulletin 17A, Guidelines for Determining Flood Flow Frequency			Revised June 1977	
























































# FEDERAL EMERGENCY MANAGEMENT AGENCY

# VOLUME 3 OF 3



# SANTA CRUZ COUNTY, CALIFORNIA AND INCORPORATED AREAS

COMMUNITY NAME	COMMUNITY NUMBER	
CAPITOLA, CITY OF	060354	
SANTA CRUZ, CITY OF	060355	
SANTA CRUZ COUNTY UNINCORPORATED AREAS	060353	
SCOTTS VALLEY, CITY OF	060356	
WATSONVILLE, CITY OF	060357	



# REVISED: SEPTEMBER 29, 2017

FLOOD INSURANCE STUDY NUMBER 06087CV003C

Version Number 2.3.2.0

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Corralitos Creek	16-19 P
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Harkins Slough	22-23 P
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Soquel Creek	67-70 P
Struve Slough	71-73 P
Thomasello Creek	74 P
Thompson Creek	75 P
Watsonville Slough	76-84 P
Zayante Creek	85-89 P

## Published Separately

Flood Insurance Rate Map (FIRM)
























































































































